

SL



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Date: April 1, 1999
From: Gregg Griffith
Subj: Alder VOC Test Results
To: Scott Inloes, SWAPCA

Scott,

Enclosed you will find Horizon Engineering's second round VOC test report for Alder drying at Centralia and Longview. Sorry it took so long to complete, but you are aware of the hold ups that occurred.

Thanks

Gregg

A handwritten signature in cursive script that appears to read "Gregg".

RECEIVED
APR -5 1999
SOUTHWEST AIR POLLUTION
CONTROL AUTHORITY



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Project No. 843

SOURCE EVALUATION TEST REPORT

NORTHWEST HARDWOODS Dry Kiln VOC Emission Factors

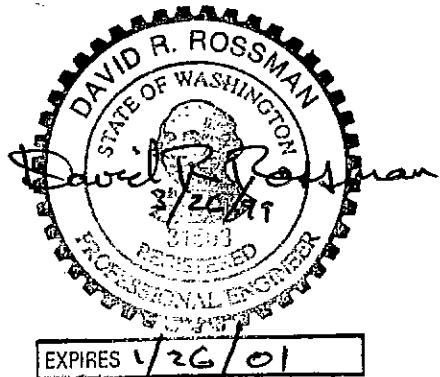
January 19-20, 1999

Prepared for

Northwest Hardwoods
3000 Galvin Road
Centralia, WA 98531

by

Kate Krisor &
David R. Rossman P.E.



Introduction

On January 19 and 20, 1999, a sample of lumber from Northwest Hardwoods was dried in Horizon Engineering's laboratory dry kiln. About 12 board feet of Alder lumber was dried. Volatile organic compounds (measured as total gaseous organic compounds, TGOC) were continuously measured in the test kiln using the Dettinger/Horizon Method. The laboratory test was done instead of a source test due to the expense and uncertainties involved in source testing an actual dry kiln.

Although Alder had been test-dried before, this test was required by SWAPCA to determine if there is seasonal variation in VOC emissions from the wood.

Greg S. Griffith of Northwest Hardwoods arranged for the work and prepared the lumber sample. Horizon Engineering personnel David Broderick did the testing and Michael Wallace assisted in the data processing. A copy of the original test method has been included in the Appendix.

Summary of Results

Table 1 summarizes the results of the testing. Figure 1 is a plot of the calculated emission factors for the range of percentage H₂O (wet basis) of the wood samples. The emission factor plot ranges between 51% (raw wet boards) and 12% (dry boards). It should be noted that the results are based on an actual board-foot basis, not the nominal dimensions of each sample board.

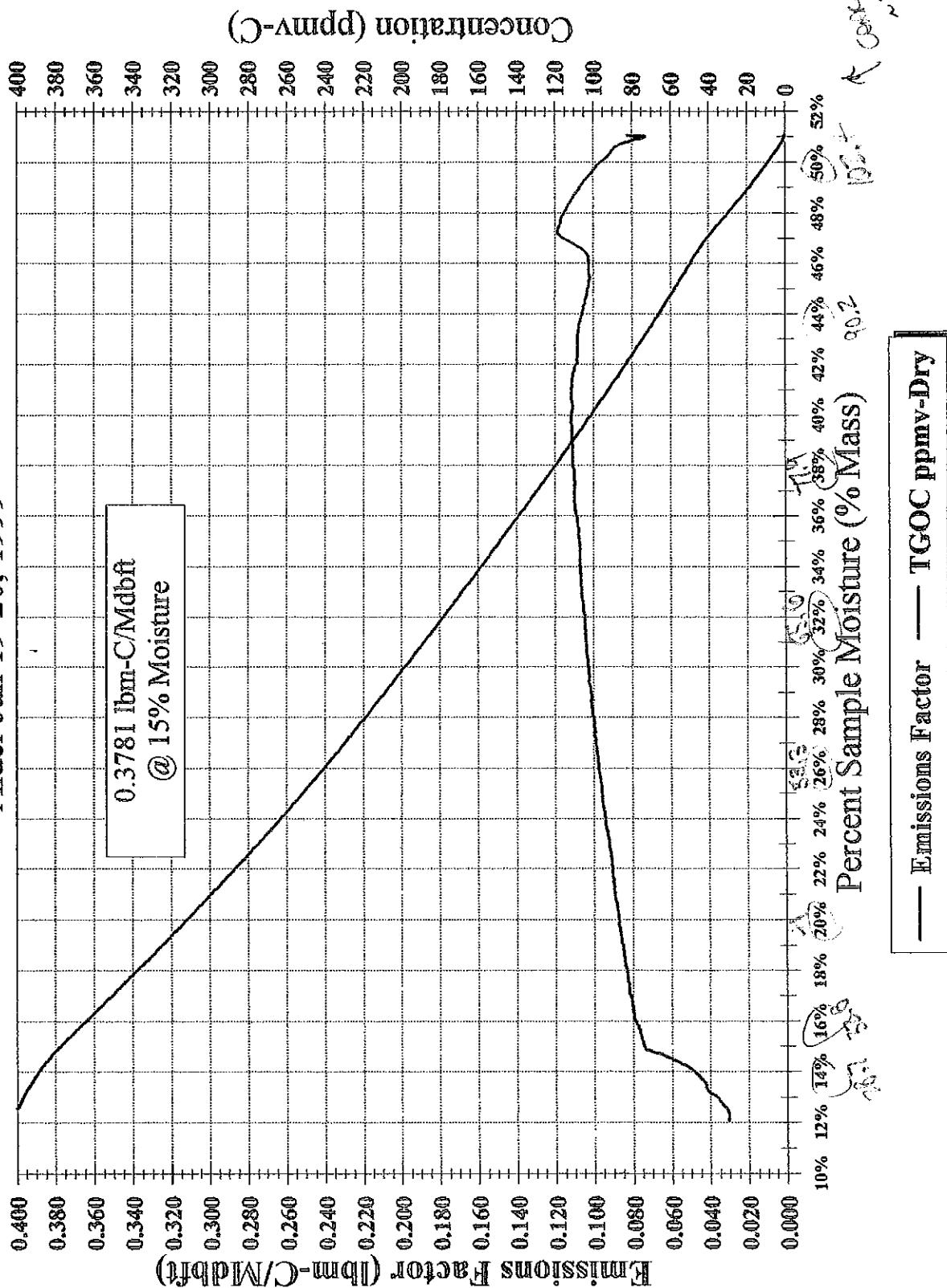
Detailed results and sampling parameters are included in the Appendix.

Table 1
Summary of Results

Results	Units	
Species		Alder
Dates		Jan. 19 & 20, 1999
Sample Size	bd ft (dry)	11.7
Initial Weight	lb	54.7
Weight Loss	lb	21.3
Test Time to 12% H ₂ O	hr	12.5
Avg VOC (Dry)	ppmvC	88
Max VOC (Wet)	ppmvC	69
Emission Factor		
@ 15% Moisture	lbC/Mbdft	0.38
@ 12% Moisture	lbC/Mbdft	0.40

Northwood Hardwoods

Alder Jan 19-20, 1999



Purpose for the Laboratory Test Method

Northwest Hardwoods uses dry kilns to dry cut lumber. Testing the actual kilns would be difficult, costly, and there would be many uncertainties when using the standard EPA Method 25A on a dry kiln. The following conditions make dry kiln testing difficult:

- a.) Lumber drying can take over 100 hours to process one load.
- b.) Most dry kilns have multiple vents and often have significant leakage around the loading doors.
- c.) The venting process is periodic. The vents open to release moisture and VOCs in an irregular pattern.

The multiple-vent configuration of most dry kilns and the periodic venting makes it difficult to quantify the total exhaust rate. Leakage from doors and other gaps is difficult to measure and would thus produce inaccurate results. Additionally, tests would need to be repeated for every species of wood the plant dries.

Sampling and Analytical Procedures

Testing Method The Dettinger/Horizon Method, applied to the test kiln, employs EPA Method 25A in a controlled manner to measure TGOC emissions. The method is assumed to be a worst case analysis, drying to the highest temperature for a normal drying cycle. The test chamber humidity is not controlled but inlet air humidity and volume rate is measured. Normal maximum temperature in a dry kiln is about 200°F but this varies for species and by kiln site. This method allows sample drying times of approximately 36 to 48 hours. Actual drying cycles may take between 36 to over 100 hours.

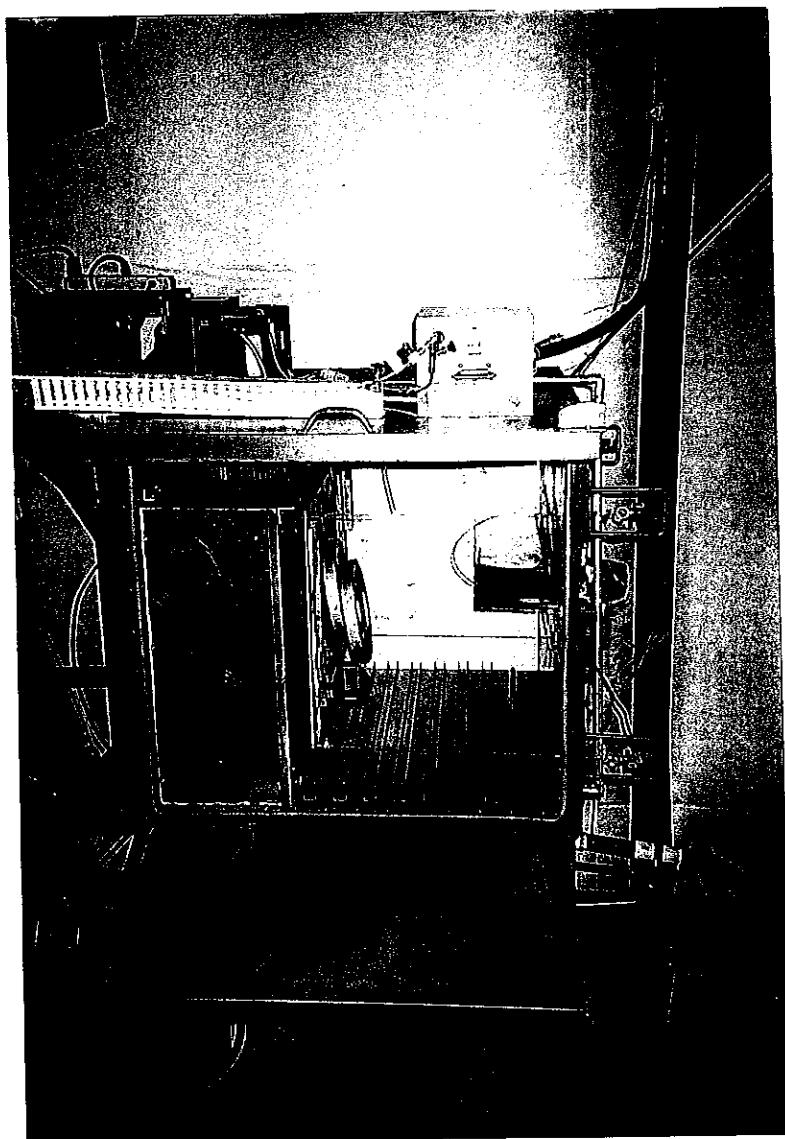
We refined the Dettinger/Horizon Method for this work to obtain dry air flow rates from moisture data rather than measurement of in-flow air. This is described in detail in the flow rate section below.

General The test kiln schematic is in the Test Method in the Appendix. A Grieve 27-ft³ industrial convection oven was used to dry the wood. Four Rice Lake Weighing Systems 0-100 lb load cells are used to continuously monitor the weight of the drying lumber. Figure 2 shows the kiln during calibrations of the load cells. Weight loss (moisture loss) was recorded until a stable weight was

recorded, indicating that the load was dry. Temperatures were monitored with k-type thermocouples.

Test parameters were read every 30 seconds during the tests by a Keithley Metrabyte DAS-801 data acquisition board installed in a personal computer and customized with Test Point programming software. Data acquisition system (DAS) printouts are in the Appendix.

Figure 2
Test Kiln, with Load Cell Calibration Weights



VOC A J.U.M. Engineering VE-7 total hydrocarbon analyzer with heated flame ionization detector and heated sample line was used to measure TGOC concentrations at oven conditions. Gas sample for the analyzer was taken from a fixed sampling probe in the oven. The analyzer output was read every 30 seconds and two-minute averages were recorded by the DAS. Emission factors were only calculated down to 12% moisture.

Zero, span, calibration error (linearity) and bias checks were made on the TGOC monitor at the beginning and end of the test.

The VOC analyzer concentrations are corrected for minor instrument drift according to the time when calibrations were done and when the test run was made. System calibration response (bias check) values are used as the basis for these corrections.

Moisture Kiln moisture was calculated from the wet and dry bulb temperatures as indicated by k-type thermocouples. Wet bulb temperature was maintained with a wick and a reservoir supplied with water from outside the kiln. The thermocouples were monitored continuously but the outputs were read every 30 seconds and two-minute averages were recorded by the DAS.

Flow Rate The flow rate used in TGOC rate calculation was obtained from the moisture content of the air in the kiln. Knowing the percentage moisture in the kiln air and the rate that water in the lumber was evaporated in the kiln (measured by the load cells), the volume of dry air can be determined using EPA's moisture content equation, Eq. 5-3:

$$\text{MoistureContent} = \frac{\text{VolumeWater}(\text{std})}{\text{VolumeAir}(\text{std}) + \text{VolumeWater}(\text{std})}$$

Example calculations are in the Appendix.

Due to the nature of the load cells used, the lumber weight loss was not a perfectly smooth curve. The jumps in weight loss caused swings in the ongoing calculated dry air rate through the kiln. To remove these swings, a best-fit method was used to derive a smooth (conditioned) curve for the weight loss.

Board Volume The sample boards were measured individually and the board-foot amount was based on a board foot being 144 cubic inches of actual wood.

Discussion

The final moisture content (wet basis) of the actual kiln-dried lumber should be used to enter the plots of the results figures. Annual emissions of TGOC (as carbon) can be calculated based on production of dried lumber.

The quantity of VOC from this sample was about 0.40 lb/1000 bd ft at 12% moisture. The last Alder sample from Northwest Hardwoods that we processed (in August of 1996) was about 0.24 lb/1000 bd ft. at the same moisture.

APPENDIX

Nomenclature & Drift Correction Documentation

Lab Data

- Sampling Record
- Calculated Results & DAS Tables
- Example Calculations
- Temperature-Humidity Plot
- Weight-Moisture Plot

Calibration Information

- Thermocouples

Test Method

**NOMENCLATURE
AND
DRIFT CORRECTION
DOCUMENTATION**

Nomenclature

Constant	Value	s	Definition	Ref
Pstd(1)	29.92129	inHg	Standard Pressure	CRC
Pstd(2)	2116.22	lbf / ft ²		CRC
Tstd	527.67	°R	Standard Temperature	CRC
R	1545.33	ft lbf / lbmol °R	Ideal Gas Constant	CRC
MWatm	28.965	lbm / lbmole	Atmospheric (20.946 %O ₂ , 0.033% CO ₂ , Balance N ₂ +Ar)	CRC
MWc	12.011	lbm / lbmole	Carbon	CRC
MWco	28.010	lbm / lbmole	Carbon Monoxide	CRC
MWco2	44.010	lbm / lbmole	Carbon Dioxide	CRC
MWh2o	18.015	lbm / lbmole	Water	CRC
MWno2	46.006	lbm / lbmole	Nitrogen Dioxide	CRC
MWo2	31.999	lbm / lbmole	Oxygen	CRC
MWso2	64.063	lbm / lbmole	Sulfur Dioxide	CRC
MWn2+ar	28.154	lbm / lbmole (Balance with 98.82% N ₂ & 1.18% Ar)	Emission balance	
C1	385.3211	ft ³ / lbmol	Ideal Gas Constant @ Standard Conditions	
C2	816.5455	inHg in ³ /°R ft ²	Isokinetics units correction constant	
Kp	5129.4	ft / min [(inHg lbm/mole) / (°R inH ₂ O)] ^½	Pitot tube constant	Ref 2.5.1
Symbol	Units	Calculating Equation or Source of Data		
As	in ²	Area, Stack		EPA
An	in ²	Area, Nozzle		
Bws	%	Moisture, % Stack gas	[100 Vw(std) / (Vw(std)+Vm(std))]	Eq. 5-3
C	ppmv-C	Carbon (General Reporting Basis for Organics)		
C1	ft ³ /lbmol	Gas Constant @ Standard Conditions	[R Tstd / Pstd(2)]	
C2	inHg in ³ /°R ft ²		[14,400 Pstd / Tstd]	
Cd	lbm-GAS / MMdscf	Mass of gas per unit volume	[Cgas MWgas / C1]	
cg	gr/dscf	Grain Loading, Actual	[15.432 mn / Vm(std) 1,000]	Eq. 5-6
cg @ X%CO2	gr/dscf	Grain Loading Corrected to X% Carbon Dioxide	[X% / CO2%]	
cg @ X%O2	gr/dscf	Grain Loading Corrected to X% Oxygen	[(20.946-X%) / (20.946-O2%)]	
Cgas	ppmv, %	Gas Concentration, (Corrected)		
Cgas @ X%CO2	ppmv	Gas Concentration Correction to X% Carbon Dioxide	[X% / CO2%]	
Cgas @ X%O2	ppmv	Gas Concentration Correction to X% Oxygen	[(20.946-X%) / (20.946-O2%)]	
CO	ppmv	Carbon Monoxide		
Co	ft	Outer Circumference of Circular Stack		
Ci	ft	Inner Circumference of Circular Stack		
CO2	%	Carbon Dioxide		
Cp		Pitot tube coefficient		
Ct	lb/hr	Particulate Mass Emissions	[60 cg Qsd / 7,000]	
dH	in H ₂ O	Pressure differential across orifice		
Dn	in	Diameter, Nozzle		
dp ^½		Average square root of velocity pressure		
Ds	in	Diameter, Stack		
E	lb / MMBtu	Pollutant Emission Rate	Cgas Fd MWgas (20.946 / (20.946-O2%)) / (1,000,000 C1)	Table 19-1
Fd	dscf / MMBtu	F Factor for Various Fuels		
I	%	Percent Isokinetic	[C2 Ts(abs) Vm(std) / (vs Ps mfg An Ø)]	Eq. 5-8*
Md	lbm / lbmole	Molecular weight, Dry Stack Gas	[(1-%O2-%CO2)(MWn2+ar)+(%O2 MWo2)+(%CO2 MWco2) / (1-Bws/100)]	Eq. 3-1*
mfg		Mole fraction of dry stack gas		
Mgas	lbm/hr	Gaseous Mass Emissions	[60 Cgas(ppmv) MW Pstd(2) Qsd / 1,000,000 R Tstd]	
mn	mg	Particulate lab sample weight		
Ms	lbm / lbmole	Molecular weight, Wet Stack	[Md mfg +MWh2o (1-mfg)]	Eq. 2-5
MW	lbm / lbmole	Molecular Weight		
NO2	ppmv-NO2	Nitrogen Dioxide (General Reporting Basis for NOx)		
NOx	ppmv-NO2	Nitrogen Oxides (Reported as NO2)		
O2	%	Oxygen		
OPC	%	Opacity		
Pbar	in Hg	Pressure, Barometric		
Pg	in H ₂ O	Pressure, Static Stack		
Po	in Hg	Pressure, Absolute across Orifice	[Pbar+dH/13.5955]	
Ps	in Hg	Pressure, Absolute Stack	[Pbar+Pg/13.5955]	Eq. 2-6*
Qa	acf/min	Volumetric Flowrate, Actual	[As vs / 144]	
Qsd	dscf/min	Volumetric Flowrate, Dry Standard	[Qa Tstd mfg Ps] / [Pstd(1) Ts(abs)]	Eq 2-10*
Rf	MMBtu/hr		[1,000,000 Mgas (20.946-O2)] / [Cd Fd 20.946]	
SO2	ppmv-SO2	Sulfur Dioxide		
t	in	Wall thickness of a stack or duct		
TGOC	ppmv-C	Total Gaseous Organic Concentration (Reported as C)		
Tm	°F	Temperature, Dry gas meter		
Tm(abs)	°R	Temperature, Absolute Dry Meter	[Tm + 459.67]	
Ts	°F	Temperature, Stack gas		
Ts(abs)	°R	Temperature, Absolute Stack gas	[Ts + 459.67]	
Vlc	ml	Volume of condensed water		
Vm	def	Volume, Gas sample		
Vm(std)	dscf	Volume, Dry standard gas sample	[Y Vm Tstd Po] / [Pstd(1) Tm(abs)]	Eq. 5-1
vs	fpm	Velocity, Stack gas	Kp Cp dp ^½ [Ts(abs) / (Ps Ms)] ^½	Eq. 2-9*
Vw(std)	scf	Volume, Water Vapor	0.04707 Vlc	Eq. 5-2
Y		Dry gas meter calibration factor		Fig. 5.6
Ø	min	Time, Total sample		

* Based on equation.

DRIFT CORRECTION DOCUMENTATION

EPA Drift Equations

Method 3a : Oxygen and Carbon Dioxide

- [1] With low level cal. gas greater than zero. $C_{gas} = \frac{(C_{ma} - C_{oa}) * (C - C_m)}{(C_m - C_o)} + C_{ma}$; $C_{oa} > 0$ (Eq. 3a-1)
- [2] With low level cal. gas equal to zero. See equation (Eq. 6c-1) ; $C_{oa} = 0$ (Eq. 6c-1)

Method 6c : Sulfur Dioxide

$$C_{gas} = \frac{C_{ma} * (C - C_o)}{(C_m - C_o)} ; C_{oa} = 0 \quad (\text{Eq. 6c-1})$$

Method 7e : Nitrogen Oxides

Section 8, Method 7e; "Follow Section 8 of Method 6c (Eq. 6c-1)."

Method 10 : Carbon Monoxide

The EPA does not currently address Gas Filter Correlation Instruments therefore there are no current standards.

Method 25a : Total Gaseous Organic Concentration (TGOC)

This method does not mention correcting for drift although there are established limits.

Horizon Engineering Drift Correction Equations.

$$C_{gas} = \frac{(C_{id} - Z_x) * (C_{ma} - C_{oa})}{(S_x - Z_x) * R} \quad S_x = \frac{(C_{mf} - C_{mi}) * (T_x - T_{ci})}{(T_{cf} - T_{ci})} + C_{mi} ; R \text{ is for TGOC.}$$

$$T_x = (T_{te} - T_{ts}) / 2 + T_{ts} \quad Z_x = \frac{(C_{of} - C_{oi}) * (T_x - T_{ci})}{(T_{cf} - T_{ci})} + C_{oi}$$

EPA	Definition	Horizon Engineering
C_{gas}	Effluent gas concentration, dry basis (Except where stated).	C_{gas}
C_{ma}	Actual upscale calibration gas concentration.	C_{ma}
C_{oa}	Actual low calibration gas or zero.	C_{oa}
C_m	Average of initial and final system upscale calibration bias responses.	
	Initial system upscale calibration bias response.	C_{mi}
	Final system upscale calibration bias response.	C_{mf}
C_o	Average of initial and final system zero/low calibration bias responses.	
	Initial system zero/low calibration bias response.	C_{oi}
	Final system zero/low calibration bias response.	C_{of}
C	Average gas concentration indicated by gas analyzer, dry basis (C_{iw} is wet basis).	C_{id}
	Starting test time	T_{ts}
	Ending test time.	T_{te}
	Initial system bias calibration response time.	T_{ci}
	Final system bias calibration response time.	T_{cf}
	Mid-point of test time or gas sampling interval to be analyzed.	T_x
	Approximate upscale response at mid-point test time.	S_x
	Approximate zero/low response at mid-point test time.	Z_x
K	Carbon count of TGOC calibration gas.. ($CH_4 = 1$, $C_3H_8 = 3 \dots$)	K
	Carbon response factor basis on a state basis. (ie Propane carbon basis)	R

Notes of Exception:

- 1] TGOC is first recorded on a wet basis then corrected to a dry basis.
- 2] There is no standard basis of carbon. At Horizon all unknown TGOC responses are corrected to a Propane carbon basis even if the calibration gas is methane. A 1ppmv carbon propane basis will cause 1ppmv methane to be recorded as 1.037 ppmv. When spanning with methane the result is corrected to indicate a propane basis carbon count. $R = 1.037$ when spanning with methane.

09/05/97

LAB DATA

Client: Northwest Hardwoods

Species: Alder

Run: 1

Start Time: 1835

Start Date: 1-19-99

Y of meter: 983

Pbar	29.90	1007 hPa				
Date	1-19	1-20				

of boards: 10

dim of boards:

dim of total load:

Bdft (note if dry or wet):

JUM #	actual	start bias	end bias
span	84	250.6	227.8
mid	50.5	149.3	133.3
mid	27.92	83.3	73.2
zero	0	.38	-3.8
time & date	0.	18:25/1-19	10:44/1-22

I ft with
scale = 26.0



End

local
26.3 lbs

LOAD CELL	actual	start check	end check
high	50	50.0	50.12
zero	0	0.08	0.07
time & date		1827/1-19	1048/1-22

Meter Reading	Time	Date	Load Weight
498.900	1835	1-19	54.74
503.700	1852	1-19	55.18
535.3	2043*	1-19	52.06
762.7	0713 #	1-20	35.36
870.800	1118	1-20	35.22
	1212	VOC =	132.9
990.800	1548	1-20	31.42
438.2	832	1-21	28.2
580.2	1351	1-21	27.7
651.500	1632	1-21	27.7
093.200	905	1-22	26.8

To (ΔT)

-40

-45

-30

-80

-80

-90

-105

-110

-110

High Rm
VOCs →
Painting

* increased after a small amount

MC 1047

Northwest Hardwood
Alder
119-Jan-99

TGOC Concentration , Mass Emissions and Emissions Factor									
Cm ft ³	A F	B G	E	J	D	C	H	TGOC	Mass Emission Factor
VMc scf	VWc scf	Wood H2 Volume VWW scf	Inlet Air Moisture BWSi %	Psycho BWSi %	VWi scf	VMi scf	Ve wscf	Cgas(wet) ppmv	Mass TGOC Mgas lbm-C
17.31	1.25	1.06	4.61					25.99	30.36
25.84	7.12	1.38	29.15					88.80	118.40
19.32	5.20	1.16	21.22					68.61	88.33
25.839	1.250	1.107	4.613	0.000	0.000	0.000	0.164	77.9	7.9E-07
25.566	1.358	0.023	1.104	5.042	0.000	0.000	0.326	77.9	7.9E-07
25.066	1.555	0.029	1.115	5.840	0.000	0.000	0.369	76.8	8.8E-07
24.428	1.853	0.029	1.132	7.048	0.000	0.000	0.133	76.0	3.1E-07
24.141	2.035	0.029	1.133	7.774	0.000	0.000	0.055	75.2	1.3E-07
23.989	2.160	0.029	1.116	8.261	0.000	0.000	0.081	74.1	1.9E-07
23.818	2.280	0.029	1.116	8.736	0.000	0.000	0.110	72.8	2.5E-07
23.602	2.410	0.029	1.124	9.279	0.000	0.000	0.118	71.1	2.6E-07
23.379	2.548	0.029	1.127	9.827	0.000	0.000	0.121	69.6	2.6E-07
23.144	2.690	0.029	1.117	10.414	0.000	0.000	0.123	68.6	2.6E-07
22.894	2.847	0.029	1.122	11.060	0.000	0.000	0.109	67.9	2.3E-07
22.661	2.999	0.029	1.124	11.689	0.000	0.000	0.081	66.6	1.7E-07
22.456	3.152	0.039	1.121	12.309	0.000	0.000	0.075	65.5	1.5E-07
22.284	3.287	0.027	1.122	12.855	0.000	0.000	0.048	64.5	9.7E-08
22.135	3.414	0.023	1.128	13.364	0.000	0.000	0.040	63.5	7.9E-08
22.017	3.516	0.037	1.113	13.772	0.000	0.000	0.053	63.0	1.0E-07
21.897	3.619	0.044	1.135	14.184	0.000	0.000	0.046	62.8	9.0E-08
21.804	3.710	0.085	1.146	14.542	0.000	0.000	0.095	62.4	1.8E-07
21.701	3.803	0.108	1.156	14.911	0.000	0.000	0.161	62.0	3.1E-07
21.541	3.911	0.112	1.161	15.365	0.000	0.000	0.190	61.9	3.7E-07
21.334	4.039	0.147	1.169	15.919	0.000	0.000	0.234	61.5	4.5E-07
21.089	4.197	0.212	1.167	16.597	0.000	0.000	0.309	61.7	5.9E-07
20.828	4.362	0.247	1.173	17.316	0.001	0.004	0.415	62.2	8.0E-07
20.551	4.535	0.286	1.190	18.078	0.004	0.325	0.672	63.1	1.3E-06
20.330	4.699	0.405	1.198	18.775	0.011	0.928	1.382	64.0	2.8E-06
20.144	4.848	0.471	1.206	19.397	0.016	1.271	1.779	64.8	3.6E-06
19.991	4.979	0.467	1.225	19.940	0.016	1.259	1.756	66.1	3.6E-06
19.854	5.103	0.530	1.237	20.448	0.020	1.613	2.163	67.1	4.5E-06
19.754	5.202	0.580	1.253	21.844	0.022	1.758	2.372	67.9	5.0E-06
19.645	5.300	0.593	1.245	21.248	0.022	1.749	2.368	68.8	5.1E-06
19.539	5.402	0.630	1.249	21.661	0.025	1.955	2.611	69.4	5.7E-06
19.456	5.483	0.678	1.262	21.984	0.030	2.308	3.003	69.8	6.5E-06
19.426	5.525	0.704	1.246	22.143	0.029	2.273	2.993	70.1	6.5E-06
19.376	5.587	0.710	1.245	22.382	0.029	2.325	3.050	70.5	6.7E-06
19.339	5.638	0.756	1.237	22.572	0.031	2.501	3.271	70.5	7.2E-06
19.313	5.682	0.742	1.231	22.732	0.029	2.355	3.121	71.1	6.9E-06
19.263	5.737	0.748	1.230	22.948	0.028	2.247	3.032	71.1	6.7E-06
19.183	5.809	0.784	1.232	23.242	0.030	2.405	3.237	71.8	7.2E-06
19.111	5.863	0.849	1.240	23.476	0.032	2.561	3.466	72.4	7.8E-06
19.028	5.922	0.853	1.253	23.734	0.033	2.581	3.486	73.0	7.9E-06
18.959	5.973	0.903	1.266	23.956	0.037	2.858	3.801	73.7	8.7E-06
18.930	5.998	0.978	1.269	24.061	0.039	3.068	4.085	74.5	9.5E-06
18.900	6.028	1.022	1.266	24.181	0.040	3.157	4.225	74.9	9.9E-06
18.860	6.063	1.070	1.270	24.326	0.044	3.414	4.524	75.8	1.1E-05
18.852	6.074	1.134	1.257	24.368	0.046	3.609	4.780	76.2	1.1E-05
18.848	6.087	1.163	1.259	24.410	0.047	3.689	4.912	77.1	1.2E-05

Northwest Hardwood
Alder

Start Time End Time Interval	Time min	Starting Mass		0.9830 Meter (T)		TGOC analyzer calib Span		84		250.6		227.8 ppmv		19.77 Start Cal Tim		
		26.84 lbn		29.9000 inHg		101.25 kPa		Zero		50		-3.8 ppmv		22.45 End Cal Tim		
		28.10 lbn		Total Mass Displaced		Drift		Calculated		Inlet Meter		Inlet Meter		50.12 lbn		
1A	1B	2	3	4	5	6	7	8	9	10	11	12	13	14	15	18
Interval	Interval	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	M	Corrected	Wood	Wood	Wood	Inlet Water	Inlet Water	(A+B) & (F+G)
Start Time	End Time	Tc F	Twb F	Ambient F	& Meter				lbm	Mass	Water	Moisture %	%Bwc	Vw(std)	Vw(std)	DEFT
Range to 12% H2O	Min	124.52	95.77	67.45	24.46	36.32	33.41	33.45	lbm	Wma	dVw	Volume	Volume	Water Change	Water Change	30.01
	Max	196.59	156.96	77.09	87.94	53.13	54.90	54.90	lbm	Wma	lbm	Wet	Wm(wet)	inlet	inlet	DEFT
	Avg/Sum	93.8	185.95	144.19	74.66	67.20	40.34	42.90	lbm	Wma	lbm	lbm	lbm	inlet	inlet	30.01
20:08	20:10	2.0	175.31	149.67	74.15	77.31	44.95	53.99	lbm	Wma	lbm	lbm	lbm	inlet	inlet	DEFT
20:10	20:12	2.0	175.32	149.74	74.14	78.20	44.55	53.87	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:12	20:14	2.0	175.15	149.77	74.02	79.07	44.30	53.77	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.921
20:14	20:16	2.0	175.03	149.91	73.91	79.91	44.41	53.74	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.928
20:16	20:18	2.0	175.19	150.10	73.86	80.35	44.14	53.64	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.932
20:18	20:20	2.0	175.03	150.16	73.71	80.99	44.08	53.55	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.926
20:20	20:22	2.0	174.90	150.33	73.67	81.82	43.77	53.46	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:22	20:24	2.0	175.07	150.37	73.85	82.33	43.96	53.41	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:24	20:26	2.0	175.01	150.43	73.98	82.98	43.84	53.29	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:26	20:28	2.0	174.96	150.46	74.20	83.79	43.77	53.28	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:28	20:30	2.0	174.82	150.48	74.05	84.42	43.54	53.19	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:30	20:32	2.0	175.06	150.51	74.06	84.99	43.39	53.18	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:32	20:34	2.0	175.05	150.48	74.00	85.86	43.51	53.11	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:34	20:36	2.0	175.12	150.45	74.08	86.34	43.43	53.08	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:36	20:38	2.0	175.09	150.34	73.89	86.83	43.20	52.99	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:38	20:40	2.0	175.18	150.28	73.68	87.24	43.29	52.91	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:40	20:42	2.0	176.11	150.30	73.44	87.78	43.23	52.80	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:42	20:44	2.0	177.67	150.60	73.22	87.94	42.91	52.69	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:44	20:46	2.0	179.55	151.01	72.81	87.68	42.88	52.58	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:46	20:48	2.0	181.57	151.50	72.56	86.06	42.50	52.51	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:48	20:50	2.0	183.85	152.22	72.46	83.04	42.77	52.43	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:50	20:52	2.0	185.39	153.05	72.58	79.90	42.79	52.40	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:52	20:54	2.0	186.00	153.63	72.46	76.89	43.04	52.36	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:54	20:56	2.0	186.43	154.12	72.66	75.07	43.41	52.33	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:56	20:58	2.0	186.64	154.55	72.56	73.73	43.77	52.22	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
20:58	21:00	2.0	186.98	155.05	72.56	73.17	43.86	52.14	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:00	21:02	2.0	187.11	155.35	72.86	72.79	43.66	51.98	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:02	21:04	2.0	187.06	155.55	72.94	72.61	43.32	51.66	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:04	21:06	2.0	187.01	155.72	72.88	72.52	43.27	51.53	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:06	21:08	2.0	187.33	155.98	72.29	72.28	43.15	51.91	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:08	21:10	2.0	187.10	156.09	73.78	72.22	43.19	51.91	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:10	21:12	2.0	186.89	156.11	73.56	71.98	43.36	51.74	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:12	21:14	2.0	187.29	156.24	73.58	72.16	43.26	51.59	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:14	21:16	2.0	187.64	156.44	74.03	71.98	42.93	51.59	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:16	21:18	2.0	187.77	156.67	74.10	72.16	42.48	51.56	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:18	21:20	2.0	187.54	156.69	73.86	72.52	42.45	51.45	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:20	21:22	2.0	187.41	156.69	73.41	72.56	42.55	51.34	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:22	21:24	2.0	186.88	156.68	73.03	72.93	42.22	51.30	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:24	21:26	2.0	186.32	156.57	72.47	73.34	42.09	51.18	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:26	21:28	2.0	185.92	156.39	71.79	73.50	41.78	50.93	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:28	21:30	2.0	185.74	156.41	71.08	73.94	41.76	51.81	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:30	21:32	2.0	186.14	156.56	71.24	73.88	41.74	50.54	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:32	21:34	2.0	186.71	156.56	72.02	74.28	41.45	50.45	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:34	21:36	2.0	187.20	156.68	72.75	74.38	41.30	50.41	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:36	21:38	2.0	187.57	156.79	73.55	74.69	41.37	50.44	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:38	21:40	2.0	188.04	156.88	74.47	74.96	41.29	50.55	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922
21:40	21:42	2.0	188.27	156.92	75.12	75.44	41.17	50.67	lbm	Wma	lbm	lbm	lbm	inlet	inlet	24.922

Crn It ^r	TGOC Concentration , Mass Emissions									
	A	B	C	D	E	F	G	H	I	J
VMc	VWc	Wood H2	Inlet Air	Moisture	BWSi	VWi	VMi	V _e	Cgas(wet)	TGOC
dscf	scf	scf	%	%	scf	scf	dscf	wscf	ppmv	ppmv
17.31	1.25	1.06	4.61	29.15	1.16	21.22	19.52	1665.96	2147.44	5.134
25.84	7.12	1.38	458.98	5.20	6.095	1.218	1.270	24.457	0.050	3.865
19.32	5.20	1.16								
18.827	6.095	1.247	1.258	24.499	0.051	3.966	5.257	78.0	1.2E-05	103.2
18.816	6.105	1.247	24.525	0.050	3.973	5.298	79.8	1.3E-05	104.5	1.3E-04
18.814	6.114	1.279	1.247	24.621	0.049	3.868	5.183	80.6	1.3E-05	105.7
18.794	6.139	1.260	1.245	24.736	0.051	4.065	5.413	81.1	1.4E-05	107.0
18.761	6.166	1.304	1.235	24.781	0.051	4.075	5.460	81.7	1.4E-05	107.7
18.754	6.178	1.339	1.227	24.898	0.052	4.199	5.607	82.6	1.4E-05	108.7
18.729	6.209	1.350	1.217	24.920	0.052	4.197	5.604	83.1	1.5E-05	109.9
18.718	6.213	1.357	1.230	24.959	0.055	4.422	5.899	83.8	1.5E-05	110.7
18.710	6.223	1.424	1.232	24.980	0.056	4.457	5.942	84.6	1.6E-05	111.6
18.706	6.229	1.435	1.239	24.980	0.056	4.416	5.902	85.2	1.6E-05	112.7
18.706	6.234	1.422	1.226	24.996	0.055	4.416	5.902	85.2	1.6E-05	113.6
18.696	6.235	1.503	1.222	25.010	0.058	4.708	6.268	85.8	1.7E-05	114.4
18.702	6.230	1.547	1.223	24.988	0.060	4.849	6.459	86.7	1.7E-05	115.6
18.705	6.224	1.520	1.224	24.968	0.060	4.835	6.414	87.2	1.7E-05	116.2
18.723	6.208	1.533	1.210	24.900	0.059	4.856	6.453	87.7	1.8E-05	116.7
18.730	6.196	1.550	1.204	24.857	0.060	4.881	6.526	88.1	1.8E-05	117.2
18.706	6.184	1.540	1.193	24.844	0.056	4.637	6.293	88.6	1.7E-05	117.9
18.623	6.184	1.804	1.147	26.436	0.055	4.723	6.605	80.7	1.7E-05	119.7
18.514	6.206	1.545	1.175	24.996	0.054	4.526	6.198	88.8	1.7E-05	118.4
17.936	6.573	1.790	1.149	26.819	0.054	4.645	6.505	77.7	1.6E-05	106.2
17.842	6.242	1.592	1.158	25.215	0.053	4.544	6.267	88.5	1.7E-05	118.4
18.388	6.290	1.653	1.139	25.488	0.052	4.476	6.268	86.9	1.7E-05	116.6
18.220	6.371	1.741	1.142	25.907	0.052	4.498	6.350	83.9	1.7E-05	113.2
18.047	6.485	1.804	1.147	26.436	0.055	4.723	6.605	80.7	1.7E-05	117.9
17.936	6.573	1.790	1.149	27.154	0.054	4.645	6.505	77.7	1.6E-05	106.2
17.842	6.651	1.762	1.167	27.451	0.054	4.533	6.357	75.9	1.5E-05	104.1
17.763	6.721	1.727	1.172	27.451	0.051	4.315	6.107	74.5	1.4E-05	102.7
17.669	6.802	1.618	1.175	27.797	0.049	4.102	5.773	73.9	1.3E-05	102.4
17.614	6.852	1.510	1.181	28.006	0.046	3.843	5.397	73.6	1.2E-05	102.2
17.580	6.889	1.440	1.175	28.154	0.043	3.654	5.136	73.4	1.2E-05	102.1
17.550	6.920	1.440	1.171	28.279	0.042	3.576	5.071	73.3	1.2E-05	102.2
17.498	6.960	1.401	1.185	28.456	0.042	3.544	4.979	73.1	1.1E-05	102.1
17.484	6.983	1.448	1.205	28.539	0.045	3.715	5.199	73.0	1.3E-05	102.7
17.485	6.990	1.466	1.201	28.561	0.045	3.691	5.217	72.8	1.2E-05	101.9
17.453	7.006	1.535	1.199	28.645	0.046	3.793	5.387	73.0	1.2E-05	102.3
17.383	7.092	1.432	1.149	28.978	0.043	3.709	5.682	73.8	1.2E-05	103.9
17.410	7.037	1.523	1.208	28.784	0.045	3.709	5.282	72.8	1.2E-05	102.2
17.366	7.075	1.554	1.198	28.948	0.047	3.908	5.501	74.2	1.1E-05	104.4
17.367	7.083	1.544	1.188	28.970	0.047	3.902	5.488	74.4	1.1E-05	104.4
17.371	7.085	1.505	1.173	28.969	0.045	3.691	5.217	74.8	1.1E-05	105.1
17.420	7.084	1.321	1.069	28.908	0.036	3.350	4.729	74.7	1.1E-05	105.1
17.407	7.075	1.349	1.090	28.898	0.037	3.332	4.736	75.2	1.1E-05	105.7
17.414	7.082	1.388	1.124	28.911	0.041	3.636	4.976	75.3	1.1E-05	106.0
17.454	7.058	1.350	1.090	28.948	0.038	3.412	4.793	74.4	1.0E-05	104.4
17.349	7.100	1.402	1.146	29.039	0.040	3.467	4.927	75.6	1.2E-05	106.5
17.323	7.109	1.386	1.179	29.097	0.041	3.460	4.897	75.9	1.2E-05	107.0
17.312	7.111	1.202	29.115	0.042	3.458	4.886	76.3	1.2E-05	107.7	8.12E-04

Northwest Hardwood Alder 19-Jan-99										54.94 lbm Starting Mass		0.9830 Meter (Y)		TGOC analyzer calib Span Zero		84 250.6 227.8 ppmv		19.77 Start Cal Tim			
										26.84 lbm Ending Mass		29.9000 inHg 101.25 kPa		Load cell calibration Span Zero		0 0.38 -3.8 ppmv		22.45 End Cal Tim			
										28.10 lbm Total Mass Displaced				50 50 50.12 lbm		11.7/4057 30.01					
IA	1B	2	3	4	5	"Value"	"Value"	Tm	Voc	"Value"	"Value"	M	Corrected	Drift	Calculated	Wood	Wood	Inlet Meter	Inlet Meter	DBFT	Start Cal Tim
Interval	Interval	Duration	Time	Tc	Twb	RH	ppmv	F	F	M	%	lbm	Mass	Water	Change	Wbm	Wbm	Moisture	%Bwc	lbm	Chamber
Start Time	End Time	min				Ambient	& Meter					lbm	lbm	dWw	gm	lbm	lbm	Volume	Volume	lbm	30.01
Range to 12% H2O	Min	Max	93.8	124.52	196.59	144.19	156.96	77.09	87.94	53.13	54.90	54.90	54.91	33.47	0.48	12.0%	51.1%	20.84	29.4%	0.08	11.7/4057
Avg/Sum	21.44	2.0	188.10	156.95	75.11	75.40	41.75	50.72	50.74	50.750	50.750	50.750	50.750	29.79	43.5%	0.7219	0.6912	98.8%	0.1808	0.0083	24.429
21.44	2.0	188.06	156.96	74.94	75.57	41.32	50.66	50.68	50.684	50.684	50.684	50.684	29.57	43.4%	0.7219	0.6915	98.8%	0.1780	0.0084	24.431	
21.48	2.0	187.94	156.96	74.92	75.80	41.37	50.62	50.61	50.621	50.621	50.621	50.621	28.96	43.3%	0.7219	0.6916	98.8%	0.1780	0.0084	24.435	
21.50	2.0	187.72	156.87	74.78	75.79	41.01	50.52	50.55	50.556	50.556	50.556	50.556	29.13	43.2%	0.7219	0.6918	98.8%	0.1757	0.0083	24.444	
21.52	2.0	187.22	156.68	74.42	76.02	41.35	50.40	50.48	50.491	50.491	50.491	50.491	29.74	43.0%	0.7219	0.6923	98.8%	0.1752	0.0083	24.463	
21.54	2.0	186.79	156.44	74.03	76.22	41.39	50.25	50.42	50.427	50.427	50.427	50.427	29.07	42.9%	0.7219	0.6929	98.8%	0.1732	0.0082	24	
21.54	2.0	186.37	156.25	73.66	76.21	41.36	50.20	50.36	50.364	50.364	50.364	50.364	28.63	42.8%	0.7219	0.6935	98.9%	0.1711	0.0081	24.471	
21.56	2.0	185.86	156.14	73.06	76.27	41.18	50.12	50.29	50.299	50.299	50.299	50.299	29.52	42.7%	0.7219	0.6945	98.9%	0.1671	0.0079	24.514	
21.58	2.0	185.39	155.95	72.58	76.43	41.03	50.04	50.23	50.233	50.233	50.233	50.233	29.87	42.6%	0.7219	0.6953	98.9%	0.1640	0.0077	24.532	
22.00	2.0	185.35	155.85	72.72	76.58	41.08	50.03	50.16	50.168	50.168	50.168	50.168	29.68	42.4%	0.7219	0.6951	98.9%	0.1649	0.0078	24.533	
22.02	2.0	185.31	155.85	73.11	76.77	41.27	50.07	50.10	50.103	50.103	50.103	50.103	29.32	42.3%	0.7219	0.6944	98.9%	0.1677	0.0079	24.535	
22.04	2.0	185.25	155.92	73.57	76.77	41.24	50.04	50.03	50.039	50.039	50.039	50.039	29.30	42.2%	0.7219	0.6937	98.9%	0.1701	0.0080	24.537	
22.06	2.0	185.28	155.79	73.96	76.80	40.91	50.00	49.97	49.976	49.976	49.976	49.976	28.62	42.1%	0.7219	0.6932	98.9%	0.1708	0.0081	24.536	
22.08	2.0	185.37	155.85	74.16	77.20	40.74	49.95	49.91	49.917	49.917	49.917	49.917	26.48	42.0%	0.7219	0.6929	98.8%	0.1712	0.0081	24.533	
22.10	2.0	185.32	155.97	74.14	77.30	40.50	49.91	49.86	49.863	49.863	49.863	49.863	24.76	41.9%	0.7219	0.6930	98.9%	0.1701	0.0080	24.535	
22.12	2.0	185.24	155.94	73.99	77.56	40.53	49.83	49.80	49.810	49.810	49.810	49.810	23.92	41.8%	0.7219	0.6932	98.9%	0.1694	0.0080	24.537	
22.14	2.0	185.26	155.92	73.57	76.77	41.24	50.04	50.03	50.039	50.039	50.039	50.039	29.30	41.7%	0.7219	0.6931	98.9%	0.1709	0.0081	24.537	
22.16	2.0	185.28	155.79	73.96	76.80	40.91	50.00	49.97	49.976	49.976	49.976	49.976	28.62	41.6%	0.7219	0.6926	98.8%	0.1739	0.0082	24.525	
22.18	2.0	185.37	155.85	74.16	77.20	40.74	49.95	49.91	49.917	49.917	49.917	49.917	26.48	41.5%	0.7219	0.6917	98.8%	0.1770	0.0083	24.514	
22.20	2.0	186.20	156.20	75.27	78.17	40.96	49.56	49.57	49.572	49.572	49.572	49.572	29.37	41.4%	0.7219	0.6911	98.8%	0.1783	0.0084	24.501	
22.22	2.0	186.78	156.33	75.57	78.13	40.60	49.43	49.50	49.503	49.503	49.503	49.503	31.30	41.2%	0.7219	0.6931	98.9%	0.1709	0.0081	24.537	
22.24	2.0	187.10	156.39	75.73	78.18	40.38	49.38	49.43	49.433	49.433	49.433	49.433	31.76	41.1%	0.7219	0.6932	98.8%	0.1784	0.0084	24.467	
22.26	2.0	187.13	156.32	75.76	78.26	40.50	49.32	49.36	49.365	49.365	49.365	49.365	30.63	41.0%	0.7219	0.6904	98.8%	0.1783	0.0084	24.466	
22.28	2.0	186.89	156.18	75.75	78.42	40.83	49.29	49.29	49.297	49.297	49.297	49.297	30.92	40.9%	0.7219	0.6904	98.8%	0.1804	0.0085	24.475	
22.30	2.0	186.67	156.07	75.62	78.58	40.83	49.24	49.22	49.230	49.230	49.230	49.230	30.54	40.7%	0.7219	0.6906	98.8%	0.1797	0.0083	24.483	
22.32	2.0	186.20	155.97	75.70	78.46	40.59	49.13	49.16	49.165	49.165	49.165	49.165	29.76	40.6%	0.7219	0.6905	98.8%	0.1784	0.0084	24.479	
22.34	2.0	186.38	155.85	75.67	78.38	40.73	49.01	49.09	49.100	49.100	49.100	49.100	29.42	40.5%	0.7219	0.6905	98.8%	0.1783	0.0084	24.467	
22.36	2.0	186.78	155.70	75.70	78.38	40.73	49.01	49.09	49.097	49.097	49.097	49.097	30.53	40.4%	0.7219	0.6905	98.8%	0.1770	0.0085	24.466	
22.38	2.0	185.92	155.71	75.58	78.35	40.63	48.94	49.02	49.033	49.033	49.033	49.033	30.53	40.3%	0.7219	0.6905	98.8%	0.1785	0.0084	24.479	
22.40	2.0	185.71	155.73	75.51	78.33	40.76	48.87	48.96	48.966	48.966	48.966	48.966	30.25	40.2%	0.7219	0.6904	98.8%	0.1787	0.0084	24.520	
22.42	2.0	185.93	155.77	75.54	78.64	40.72	48.78	48.89	48.899	48.899	48.899	48.899	31.79	39.6%	0.7219	0.6907	98.8%	0.1788	0.0084	24.511	
22.44	2.0	186.38	155.85	75.67	78.55	40.58	48.70	48.82	48.831	48.831	48.831	48.831	30.87	40.0%	0.7219	0.6905	98.8%	0.1788	0.0084	24.494	
22.46	2.0	186.78	155.97	75.73	78.49	40.18	48.67	48.75	48.761	48.761	48.761	48.761	31.60	39.9%	0.7219	0.6905	98.8%	0.1774	0.0084	24.479	
22.48	2.0	187.22	156.06	75.79	78.73	39.61	48.61	48.69	48.693	48.693	48.693	48.693	30.85	39.8%	0.7219	0.6906	98.8%	0.1752	0.0083	24.463	
22.50	2.0	187.15	154.95	75.08	78.91	40.10	48.47	48.55	48.553	48.553	48.553	48.553	31.79	39.5%	0.7219	0.6904	98.8%	0.1787	0.0084	24.445	
22.52	2.0	186.74	154.93	75.16	79.07	39.24	47.91	48.19	48.200	48.200	48.200	48.200	32.50	38.9%	0.7219	0.6916	98.9%	0.1770	0.0080	24.435	
22.54	2.0	188.03	155.67	75.84	78.61	39.83	48.39	48.47	48.483	48.483	48.483	48.483	31.99	39.4%	0.7219	0.6904	98.8%	0.1765	0.0083	24.432	
22.56	2.0	186.27	154.92	75.12	78.88	39.63	47.85	48.12	48.127	48.127	48.127	48.127	33.38	38.7%	0.7219	0.6916	98.8%	0.1716	0.0081	24.432	
22.58	2.0	186.06	154.89	75.28	78.92	40.13	47.86	48.04	48.051	48.051	48.051	48.051	34.12	38.6%	0.7219	0.6912	98.8%	0.1747	0.0082	24.432	
22.60	2.0	186.46	154.92	75.98	78.84	39.85	47.91	47.97	48.227	48.227	48.227	48.227	31.73	39.0%	0.7219	0.6918	98.8%	0.1773	0.0083	24.445	
22.62	2.0	186.74	155.01	76.33	78.72	39.53	47.84	47.89	47.899	47.899	47.899	47.899	34.62	38.3%	0.7219	0.6903	98.8%	0.177			

Cm ft	A F	B G	E VWc scf	J Wood H2 Volume scf	I Inlet Air Moisture BWSi %	D VWI scf	C VMI dsfcf	H Ve wsfcf	TGOC Concentration , Mass Emissions and Emissions Factor
17.309	7.121	1.405	1.218	29.148	0.043	3.518	4.965	76.3	1.2E-05
17.309	7.122	1.394	1.199	29.150	0.042	3.488	4.921	76.5	1.2E-05
17.312	7.124	1.365	1.199	29.154	0.042	3.478	4.878	76.7	1.2E-05
17.331	7.112	1.374	1.184	29.096	0.043	3.578	4.976	76.7	1.2E-05
17.376	7.087	1.402	1.179	28.971	0.044	3.718	5.149	76.9	1.2E-05
17.428	7.051	1.371	1.165	28.804	0.043	3.622	5.019	77.2	1.2E-05
17.470	7.025	1.350	1.150	28.678	0.041	3.526	4.898	77.2	1.2E-05
17.500	7.014	1.392	1.122	28.614	0.042	3.709	5.125	77.2	1.2E-05
17.543	6.989	1.408	1.100	28.488	0.041	3.716	5.164	77.4	1.2E-05
17.562	6.971	1.400	1.106	28.414	0.041	3.628	5.067	77.5	1.2E-05
17.564	6.971	1.382	1.126	28.414	0.040	3.525	4.945	77.7	1.2E-05
17.551	6.986	1.382	1.143	28.471	0.043	3.681	5.106	77.7	1.2E-05
17.574	6.962	1.350	1.149	28.373	0.040	3.464	4.857	77.8	1.2E-05
17.561	6.971	1.249	1.152	28.416	0.037	3.150	4.433	78.2	1.1E-05
17.542	6.993	1.168	1.144	28.503	0.035	3.035	4.235	78.3	1.0E-03
17.548	6.989	1.128	1.139	28.485	0.033	2.901	4.063	78.6	9.33E-04
17.544	6.993	1.181	1.149	28.500	0.034	2.924	4.151	78.8	1.0E-03
17.505	7.020	1.236	1.170	28.624	0.037	3.087	4.371	79.0	1.0E-03
17.476	7.038	1.296	1.192	28.710	0.041	3.384	4.734	79.1	1.0E-03
17.482	7.019	1.385	1.202	28.647	0.042	3.477	4.926	79.2	1.0E-03
17.448	7.031	1.476	1.203	28.722	0.045	3.736	5.270	79.2	1.0E-03
17.431	7.037	1.498	1.203	28.760	0.047	3.877	5.423	79.2	1.0E-03
17.442	7.024	1.444	1.208	28.711	0.046	3.802	5.283	79.3	1.0E-03
17.442	7.003	1.458	1.217	28.614	0.047	3.829	5.326	79.5	1.0E-03
17.495	6.988	1.440	1.212	28.542	0.046	3.789	5.257	79.6	1.0E-03
17.524	6.977	1.403	1.208	28.477	0.046	3.783	5.221	79.5	1.0E-03
17.566	6.947	1.387	1.212	28.341	0.045	3.661	5.090	79.5	1.0E-03
17.577	6.938	1.440	1.204	28.302	0.046	3.745	5.226	79.4	1.0E-03
17.486	6.977	1.455	1.182	28.520	0.046	3.840	5.358	79.8	1.0E-03
17.576	6.944	1.426	1.205	28.319	0.045	3.704	5.184	79.4	1.0E-03
17.565	6.946	1.437	1.205	28.338	0.045	3.694	5.193	79.7	1.0E-03
17.540	6.954	1.456	1.206	28.391	0.045	3.708	5.224	79.6	1.0E-03
17.511	6.968	1.490	1.197	28.465	0.046	3.802	5.355	79.6	1.0E-03
17.486	6.977	1.455	1.182	27.859	0.046	4.001	5.558	80.1	1.0E-03
17.492	6.953	1.499	1.188	28.445	0.048	4.001	5.551	80.1	1.0E-03
17.510	6.925	1.499	1.200	28.341	0.049	4.049	5.600	79.6	1.0E-03
17.539	6.893	1.509	1.191	28.214	0.050	4.136	5.681	79.7	1.0E-03
17.707	6.791	1.574	1.157	27.720	0.050	4.252	5.858	80.0	1.0E-03
17.717	6.789	1.609	1.178	27.704	0.051	4.317	5.953	80.1	1.0E-03
17.703	6.788	1.613	1.152	27.859	0.049	4.195	5.737	80.0	1.0E-03
17.683	6.782	1.496	1.134	27.721	0.046	4.024	5.551	80.1	1.0E-03
17.695	6.786	1.532	1.147	27.719	0.048	4.119	5.695	80.2	1.0E-03
17.677	6.794	1.632	1.196	27.765	0.053	4.352	6.038	79.9	1.0E-03
17.655	6.796	1.632	1.196	27.794	0.055	4.505	6.203	79.9	1.0E-03
17.674	6.765	1.634	1.182	27.682	0.054	4.481	6.174	80.0	1.0E-03
17.688	6.748	1.593	1.165	27.616	0.052	4.396	6.018	79.8	1.0E-03

Northwest Hardwood

54.94 lbm	Starting Mass	0.9830 Meter (Y)	TGOC analyzer calib	Span	84	250.6	227.8 ppmv
26.84 lbm	Ending Mass	29.9000 inHg	Zero	0	0	0.38	-3.8 ppmv
28.10 lbm	Total Mass Displaced	101.25 kPa	Load cell calibration	Span	50	50	50.12 lbm

Start Time	End Time	Interval	Duration	"Value"	"Value"	"Value"	"Value"	RH %	VOC ppmv	"Value"	"Value"	M lbm	Corrected Mass Wm	Mass Wm	Wood Water Change dWw	Wood Water Change dWw	Wood Water Change dVm	Wood Volume Vm(wet)	Water Volume Vm(dry)	Inlet Meter	Inlet Meter	Inlet Air Volume Vm(std)	Inlet Air Fraction dry mfg(inlet) dscf	Inlet Meter	Inlet Water Change gm	Inlet Water Volume Vw(std)	Inlet Water Change gm	(A+B) & (F+G)	Vc(x) wscf	DBFT	Start/Cat Tim	End Cat Tim	Chamber 30.01							
Range to 12% H2O	Min	Max	Avg/Sum	124.52	95.77	67.45	24.46	36.32	33.41	33.45	33.47	0.48	12.0%	54.90	54.91	38.26	51.1%	42.98	20.84	29.4%	0.7219	0.6911	98.8%	0.1710	0.0081	24.456	24.474	27.09	24.52											
23:16	23:18	2.0	187.39	154.71	75.52	78.42	38.98	47.46	47.59	47.600	32.70	37.8%	0.7219	0.6914	98.9%	0.1704	0.0080	23:20	23:22	2.0	186.92	154.55	75.34	78.53	39.06	47.40	47.52	32.50	37.6%	0.7219	0.6914	98.8%	0.1706	0.0080	24.480	24.479	27.09	24.52		
23:18	23:20	2.0	186.75	154.36	75.30	78.71	39.17	47.30	47.45	47.455	33.23	37.5%	0.7219	0.6914	98.9%	0.1704	0.0080	23:22	23:24	2.0	186.78	154.21	75.37	78.37	38.53	47.26	47.38	32.20	37.4%	0.7219	0.6914	98.9%	0.1682	0.0079	24.479	24.470	27.09	24.52		
23:22	23:24	2.0	187.03	154.21	75.58	78.53	39.08	47.23	47.30	47.313	32.13	37.2%	0.7219	0.6910	98.8%	0.1718	0.0081	23:24	23:26	2.0	187.40	154.35	76.32	78.47	39.76	47.27	47.23	32.81	37.1%	0.7219	0.6897	98.8%	0.1789	0.0084	24.470	24.471	27.09	24.52		
23:24	23:26	2.0	187.30	154.35	76.24	78.64	39.66	47.14	47.16	47.168	32.96	37.0%	0.7219	0.6898	98.8%	0.1779	0.0084	23:26	23:28	2.0	187.73	154.43	75.81	78.63	39.35	47.09	47.09	32.24	36.9%	0.7219	0.6906	98.8%	0.1742	0.0082	24.471	24.472	27.09	24.52		
23:26	23:28	2.0	187.49	154.31	75.81	78.63	39.35	47.09	47.09	47.097	32.73	36.7%	0.7219	0.6903	98.8%	0.1769	0.0083	23:28	23:30	2.0	187.53	154.37	75.93	78.40	47.03	47.02	47.02	32.73	36.7%	0.7219	0.6902	98.8%	0.1762	0.0083	24.451	24.452	27.09	24.52		
23:28	23:30	2.0	187.59	154.37	75.93	78.63	39.80	47.03	47.03	47.030	32.89	36.6%	0.7219	0.6902	98.8%	0.1745	0.0082	23:30	23:32	2.0	187.59	154.37	75.93	78.63	39.80	47.03	47.03	32.89	36.6%	0.7219	0.6902	98.8%	0.1756	0.0083	24.449	24.450	27.09	24.52		
23:30	23:32	2.0	187.53	154.37	75.93	78.63	39.80	47.03	47.03	47.030	32.89	36.6%	0.7219	0.6902	98.8%	0.1759	0.0083	23:32	23:34	2.0	187.43	154.38	76.02	78.63	39.55	46.94	46.953	32.89	36.6%	0.7219	0.6902	98.8%	0.1736	0.0082	24.451	24.452	27.09	24.52		
23:32	23:34	2.0	187.43	154.38	76.02	78.63	39.55	46.94	46.94	46.953	32.89	36.6%	0.7219	0.6902	98.8%	0.1762	0.0083	23:34	23:36	2.0	187.43	154.22	75.75	78.56	39.51	46.88	46.884	31.34	36.5%	0.7219	0.6902	98.8%	0.1745	0.0082	24.455	24.456	27.09	24.52		
23:34	23:36	2.0	187.43	154.22	75.75	78.56	39.51	46.88	46.88	46.884	31.34	36.5%	0.7219	0.6902	98.8%	0.1745	0.0082	23:36	23:38	2.0	187.57	153.96	75.78	78.58	39.71	46.80	46.81	30.58	36.3%	0.7219	0.6906	98.8%	0.1756	0.0083	24.449	24.450	27.09	24.52		
23:36	23:38	2.0	187.57	153.96	75.78	78.58	39.71	46.80	46.81	46.816	30.58	36.3%	0.7219	0.6906	98.8%	0.1759	0.0083	23:38	23:40	2.0	187.73	153.87	75.87	78.53	39.67	46.65	46.748	31.18	36.2%	0.7219	0.6904	98.8%	0.1759	0.0083	24.443	24.444	27.09	24.52		
23:38	23:40	2.0	187.59	153.87	75.87	78.53	39.67	46.65	46.65	46.748	31.18	36.2%	0.7219	0.6904	98.8%	0.1759	0.0083	23:40	23:42	2.0	187.53	153.87	75.87	78.53	39.67	46.65	46.748	31.18	36.2%	0.7219	0.6904	98.8%	0.1759	0.0083	24.443	24.444	27.09	24.52		
23:40	23:42	2.0	187.53	153.87	75.87	78.53	39.67	46.65	46.65	46.748	31.18	36.2%	0.7219	0.6904	98.8%	0.1759	0.0083	23:42	23:44	2.0	187.40	153.70	75.59	78.52	39.48	46.48	46.557	46.681	30.29	36.1%	0.7219	0.6909	98.8%	0.1728	0.0083	24.443	24.444	27.09	24.52	
23:42	23:44	2.0	187.40	153.70	75.59	78.52	39.48	46.48	46.48	46.557	46.681	30.29	36.1%	0.7219	0.6909	98.8%	0.1728	0.0083	23:44	23:46	2.0	187.21	153.55	75.46	78.34	38.96	46.36	46.614	46.620	30.32	36.0%	0.7219	0.6912	98.8%	0.1762	0.0083	24.445	24.446	27.09	24.52
23:44	23:46	2.0	187.38	153.48	75.46	78.25	38.79	46.26	46.54	46.547	30.72	35.8%	0.7219	0.6910	98.8%	0.1707	0.0080	23:46	23:48	2.0	187.25	153.55	75.70	78.12	39.09	46.21	46.447	46.476	30.68	35.2%	0.7219	0.6908	98.8%	0.1724	0.0081	24.446	24.447	27.09	24.52	
23:46	23:48	2.0	187.31	153.48	75.86	78.02	38.98	46.18	46.40	46.406	31.68	35.6%	0.7219	0.6906	98.8%	0.1724	0.0081	23:48	23:50	2.0	187.31	153.23	75.38	78.02	38.54	46.06	46.072	46.072	30.36	35.0%	0.7219	0.6914	98.9%	0.1683	0.0079	24.446	24.447	27.09	24.52	
23:48	23:50	2.0	187.31	153.23	75.38	78.02	38.54	46.06	46.06	46.000	46.007	30.36	34.5%	0.7219	0.6905	98.8%	0.1723	0.0081	23:50	23:52	2.0	187.37	153.47	75.91	77.69	38.79	46.12	46.333	46.338	30.97	35.5%	0.7219	0.6912	98.8%	0.1706	0.0080	24.446	24.447	27.09	24.52
23:50	23:52	2.0	187.31	153.47	75.91	77.69	38.79	46.12	46.12	46.333	46.338	30.97	35.5%	0.7219	0.6912	98.8%	0.1717	0.0081	23:52	23:54	2.0	187.38	153.47	75.79	78.00	38.76	46.07	46.19	46.203	30.68	35.2%	0.7219	0.6907	98.8%	0.1714	0.0081	24.447	24.448	27.09	24.52
23:52	23:54	2.0	187.38	153.47	75.79	78.00	38.76	46.07	46.07	46.19	46.203	30.68	35.2%	0.7219	0.6907	98.8%	0.1714	0.0081	23:54	23:56	2.0	187.38	153.41	75.79	78.00	38.76	46.07	46.19	46.203	30.68	35.2%	0.7219	0.6907	98.8%	0.1714	0.0081	24.447	24.448	27.09	24.52
23:54	23:56	2.0	187.31	153.41	75.79	78.00	38.76	46.07	46.07	46.19	46.203	30.68	35.2%	0.7219	0.6907	98.8%	0.1714	0.0081	23:56	23:58	2.0	187.27	153.32	75.75	77.84	38.57	46.01	46.13	46.136	30.10	35.1%	0.7219	0.6910	98.9%	0.1707	0.0081	24.446	24.447	27.09	24.52
23:56	23:58	2.0	187.27	153.32	75.75	77.84	38.57	46.01	46.01	46.007	46.007	30.10	35.1%	0.7219	0.6908	98.8%	0.1724	0.0081	23:58	23:60	2.0	186.98	153.17	75.95	77.49	38.47	45.65	45.80	45.805	30.60	34.5%	0.7219	0.6905	98.9%	0.1683	0.0079	24.446	24.447	27.09	24.52
23:58	23:60	2.0	186.98	153.17	75.95	77.49	38.47	45.65	45.65	45.600	45.607	30.60	34.5%	0.7219	0.6905	98.8%	0.1723	0.0081	23:60	23:62	2.0	186.91	153.15	75.74	77.54	38.46	45.58	45.73	45.737	30.97	34.4%	0.7219	0.6901	98.8%	0.1699	0.0080	24.446	24.447	27.09	24.52
23:60	23:62	2.0	186.91	153.15																																				

TGOC Concentration, Mass Emissions											
and Emissions Factor											
Cin ft ³	A F	B G	E VWc scf	J Wood H2 Volume VWW scf	I Inlet Air Moisture BWSi %	D Psycho BWSc %	C VWI scf	H VMi dscf	V Ve wscf	G Cgas(wet) ppmv	H Mass TGOC lbm-C
VMc dscf	VWc scf	VW scf	VWW scf	Wood H2 Volume VWW scf	Inlet Air Moisture BWSi %	Psycho BWSc %	VWI scf	VMi dscf	Ve wscf	Cgas(wet) ppmv	Mass TGOC lbm-C
17.31	1.25	25.84	7.12	1.38	29.15	4.61	21.22	19.52	1665.96	2147.44	25.99
19.32	5.20	458.98	1.16	1.16	21.22	4.61	1.16	1.16	88.80	118.40	30.36
									68.61	88.33	
											0.40
17.721	6.735	1.542	1.153	27.539	0.050	4.295	5.859	79.6	1.5E-05	109.8	1.43E-03
17.758	6.716	1.533	1.149	27.443	0.050	4.332	5.909	79.7	1.5E-05	109.9	1.45E-03
17.795	6.686	1.567	1.150	27.310	0.051	4.426	6.046	79.9	1.5E-05	109.9	1.46E-03
17.819	6.660	1.518	1.134	27.205	0.048	4.196	5.772	79.6	1.4E-05	109.3	1.48E-03
17.844	6.656	1.515	1.158	27.201	0.048	4.088	5.664	79.7	1.4E-05	109.5	1.49E-03
17.873	6.673	1.547	1.208	27.286	0.051	4.207	5.818	79.8	1.4E-05	109.6	1.51E-03
17.762	6.681	1.554	1.201	27.334	0.053	4.358	5.956	79.8	1.5E-05	109.9	1.52E-03
17.787	6.665	1.520	1.175	27.257	0.049	4.148	5.719	79.8	1.4E-05	109.8	1.53E-03
17.777	6.674	1.544	1.194	27.295	0.051	4.233	5.824	79.6	1.4E-05	109.5	1.55E-03
17.777	6.678	1.551	1.189	27.307	0.053	4.395	5.999	79.9	1.5E-05	109.8	1.56E-03
17.804	6.650	1.478	1.178	27.195	0.051	4.303	5.837	79.8	1.5E-05	109.6	1.58E-03
17.847	6.603	1.442	1.185	27.006	0.049	4.106	5.604	79.8	1.4E-05	109.3	1.59E-03
17.859	6.585	1.470	1.187	26.938	0.051	4.245	5.754	79.8	1.4E-05	109.2	1.61E-03
17.894	6.582	1.428	1.171	26.832	0.049	4.141	5.611	79.8	1.4E-05	109.0	1.62E-03
17.923	6.539	1.430	1.150	26.732	0.048	4.095	5.573	79.6	1.4E-05	108.6	1.63E-03
17.933	6.529	1.448	1.151	26.691	0.047	4.063	5.560	79.5	1.4E-05	108.4	1.65E-03
17.923	6.539	1.521	1.163	26.731	0.051	4.368	5.943	79.4	1.5E-05	108.3	1.66E-03
17.933	6.526	1.494	1.166	26.681	0.050	4.260	5.807	79.3	1.4E-05	108.1	1.68E-03
17.935	6.522	1.460	1.163	26.666	0.049	4.141	5.611	79.8	1.4E-05	108.0	1.69E-03
17.934	6.524	1.443	1.159	26.674	0.049	4.153	5.646	79.2	1.4E-05	108.6	1.70E-03
17.944	6.512	1.446	1.157	26.627	0.049	4.190	5.622	79.3	1.4E-05	108.0	1.72E-03
17.962	6.498	1.420	1.150	26.566	0.048	4.115	5.571	79.1	1.4E-05	107.7	1.73E-03
17.933	6.488	1.385	1.135	26.514	0.046	4.024	5.442	78.8	1.3E-05	107.3	1.75E-03
17.998	6.476	1.389	1.146	26.462	0.046	3.982	5.425	78.8	1.3E-05	107.7	1.69E-03
17.991	6.475	1.433	1.146	26.467	0.048	4.100	5.577	78.7	1.4E-05	108.0	1.71E-03
17.996	6.479	1.435	1.152	26.478	0.048	4.123	5.604	78.8	1.4E-05	107.0	1.77E-03
17.994	6.478	1.443	1.154	26.473	0.049	4.197	5.638	78.8	1.4E-05	107.1	1.79E-03
17.999	6.464	1.461	1.165	26.426	0.050	4.273	5.792	78.9	1.4E-05	107.2	1.80E-03
18.007	6.448	1.496	1.159	26.367	0.052	4.433	5.977	79.1	1.5E-05	107.5	1.82E-03
18.032	6.426	1.450	1.157	26.272	0.050	4.285	5.759	78.9	1.4E-05	107.0	1.84E-03
18.045	6.409	1.432	1.150	26.207	0.050	4.295	5.782	79.0	1.4E-05	107.1	1.86E-03
18.068	6.381	1.444	1.147	26.100	0.049	4.253	5.740	78.9	1.4E-05	106.7	1.87E-03
18.084	6.378	1.420	1.143	26.079	0.048	4.185	5.645	79.0	1.4E-05	106.8	1.89E-03
18.090	6.372	1.293	1.149	26.060	0.045	3.877	5.270	78.9	1.3E-05	106.6	1.90E-03
18.071	6.381	1.336	1.155	26.096	0.045	3.877	5.235	78.7	1.3E-05	106.6	1.91E-03
18.078	6.374	1.300	1.163	26.068	0.045	3.836	5.180	78.8	1.3E-05	106.5	1.93E-03
18.084	6.370	1.272	1.161	26.050	0.044	3.736	5.045	78.8	1.2E-05	106.6	1.94E-03
18.089	6.376	1.294	1.157	26.049	0.044	3.765	5.119	78.8	1.3E-05	105.8	2.00E-03
18.069	6.374	1.294	1.166	26.076	0.045	3.805	5.150	78.6	1.3E-05	106.3	1.95E-03
18.066	6.370	1.266	1.164	26.068	0.045	3.860	5.164	78.6	1.3E-05	106.3	1.96E-03
18.088	6.370	1.284	1.159	25.944	0.046	3.885	5.205	78.6	1.3E-05	106.2	1.99E-03
18.129	6.325	1.294	1.157	25.866	0.045	3.872	5.223	78.5	1.3E-05	105.8	2.01E-03
18.127	6.315	1.293	1.172	25.838	0.046	3.884	5.211	78.4	1.3E-05	105.7	2.03E-03
18.143	6.298	1.250	1.154	25.768	0.046	3.957	5.241	78.2	1.3E-05	105.4	2.04E-03
18.199	6.254	1.285	1.136	25.575	0.046	3.969	5.303	78.2	1.3E-05	105.1	2.05E-03
18.218	6.233	1.281	1.149	25.492	0.045	3.872	5.211	78.3	1.3E-05	105.1	2.07E-03
18.207	6.231	1.282	1.159	25.496	0.047	4.018	5.346	78.3	1.3E-05	105.1	2.17E-03

Northwest Hardwood Alder 19-Jan-99 new/dub												54.94 lbm	Starting Mass	29,9000 inHg	TGO/C analyzer calib	Span Zero	84	250.6	227.8 ppmv	-3.8 ppmv	19.77 Start Cal Tim	
												26.84 lbm	Ending Mass	101.25 kPa	Load cell calibration	Span Zero	50	50	50.12 lbm	DBFT	22.45 End Cal Tim	
												28.10 lbm	Total Mass Displaced			0	0.08	0.07 lbm	V(w/std)	Chamber 30.01		
IA	IB	2	3	4	5	6	"Value"	"Value"	"Value"	"Value"	"Value"	Min	Max	Ambient & Meter	Wood Water	Meter	Inlet Meter	Volume	Inlet Air	Inlet Water	(A+B) & (F+G)	
Interval Start Time	Interval End Time	Duration min	Tc F	Tm F	VOC ppmv	RH %	M lbm	M lbm	Corrected M lbm	Drift M lbm	Wood Change dWw	Wood Change dWw	Moisture %Bwc	%Bwc	Reading cuff dVm ft*	Volume Wet	Vm(wet) ft*	Volume Dry	Fraction dr mfg(inlet)	Volume Change gm	Vc(x) wscf	
Range to 12% H2O																						
00:50	00:52	2.0	187.84	151.61	75.83	76.79	38.40	44.36	44.49	44.49	27.12	27.12	32.1%	32.1%	0.7219	0.6907	98.9%	0.1701	0.0080	24.439		
	00:52	00:54	2.0	187.51	151.47	75.65	76.65	38.21	44.24	44.42	44.435	28.04	28.04	32.0%	32.0%	0.7219	0.6911	98.9%	0.1683	0.0079	24.452	
	00:54	00:56	2.0	187.65	151.64	75.99	76.67	38.41	44.26	44.36	44.374	27.83	27.83	31.9%	31.9%	0.7219	0.6905	98.8%	0.1710	0.0081	24.446	
	00:56	00:58	2.0	187.68	151.59	76.03	76.59	38.35	44.23	44.30	44.313	27.56	27.56	31.8%	31.8%	0.7219	0.6904	98.8%	0.1710	0.0081	24.445	
	00:58	01:00	2.0	187.44	151.51	75.87	76.48	38.29	44.12	44.24	44.252	27.62	27.62	31.7%	31.7%	0.7219	0.6907	98.9%	0.1698	0.0080	24.454	
	01:00	01:02	2.0	187.42	151.53	76.10	76.67	38.30	44.09	44.18	44.193	26.89	26.89	31.6%	31.6%	0.7219	0.6903	98.8%	0.1711	0.0081	24.	
	01:02	01:04	2.0	187.82	151.57	76.42	76.33	38.25	44.10	44.13	44.137	25.52	25.52	31.5%	31.5%	0.7219	0.6898	98.8%	0.1726	0.0081	24.44-	
	01:04	01:06	2.0	187.71	151.43	76.05	76.44	38.20	43.98	44.07	44.080	25.68	25.68	31.4%	31.4%	0.7219	0.6894	98.8%	0.1704	0.0080	24.444	
	01:06	01:08	2.0	187.53	151.45	76.00	76.37	38.21	43.88	44.01	44.022	26.29	26.29	31.3%	31.3%	0.7219	0.6905	98.9%	0.1701	0.0080	24.451	
	01:08	01:10	2.0	187.75	151.49	76.30	76.30	38.28	43.84	43.95	43.966	25.72	25.72	31.1%	31.1%	0.7219	0.6900	98.8%	0.1721	0.0081	24.442	
	01:10	01:12	2.0	187.69	151.39	76.13	76.27	38.09	43.74	43.90	43.909	25.87	25.87	31.0%	31.0%	0.7219	0.6903	98.9%	0.1703	0.0080	24.445	
	01:12	01:14	2.0	187.52	151.28	75.90	76.20	38.40	43.71	43.84	43.850	26.46	26.46	30.9%	30.9%	0.7219	0.6906	98.8%	0.1705	0.0080	24.451	
	01:14	01:16	2.0	187.62	151.23	76.24	76.12	37.99	43.71	43.78	43.791	26.96	26.96	30.8%	30.8%	0.7219	0.6902	98.8%	0.1705	0.0080	24.447	
	01:16	01:18	2.0	187.73	151.10	76.17	76.13	38.01	43.64	43.72	43.731	27.20	27.20	30.7%	30.7%	0.7219	0.6903	98.9%	0.1702	0.0080	24.443	
	01:18	01:20	2.0	187.65	150.97	76.08	76.21	38.21	43.60	43.66	43.673	26.37	26.37	30.6%	30.6%	0.7219	0.6904	98.8%	0.1706	0.0080	24.446	
	01:20	01:22	2.0	187.67	150.81	76.10	76.31	38.36	43.58	43.60	43.615	26.25	26.25	30.5%	30.5%	0.7219	0.6903	98.8%	0.1713	0.0081	24.445	
	01:22	01:24	2.0	187.57	150.68	76.17	76.08	38.30	43.50	43.54	43.556	26.99	26.99	30.4%	30.4%	0.7219	0.6902	98.8%	0.1724	0.0081	24.449	
	01:24	01:26	2.0	187.41	150.61	75.97	76.05	38.33	43.44	43.48	43.495	27.46	27.46	30.3%	30.3%	0.7219	0.6905	98.8%	0.1705	0.0080	24.455	
	01:26	01:28	2.0	187.52	150.64	75.87	76.07	38.29	43.37	43.42	43.436	26.89	26.89	30.2%	30.2%	0.7219	0.6907	98.9%	0.1698	0.0080	24.451	
	01:28	01:30	2.0	187.35	150.53	75.68	76.05	38.16	43.27	43.36	43.375	27.56	27.56	30.1%	30.1%	0.7219	0.6910	98.9%	0.1682	0.0079	24.458	
	01:30	01:32	2.0	187.41	150.45	75.65	75.63	38.07	43.21	43.30	43.311	29.39	29.39	30.0%	30.0%	0.7219	0.6911	98.9%	0.1677	0.0079	24.456	
	01:32	01:34	2.0	187.47	150.42	75.61	75.72	38.12	43.12	43.24	43.248	28.44	28.44	29.8%	29.8%	0.7219	0.6902	98.9%	0.1724	0.0081	24.453	
	01:34	01:36	2.0	187.47	150.38	75.75	75.65	38.46	43.02	43.17	43.186	27.92	27.92	29.7%	29.7%	0.7219	0.6909	98.9%	0.1699	0.0080	24.453	
	01:36	01:38	2.0	187.37	150.26	75.94	75.58	38.49	42.96	43.11	43.124	28.37	28.37	29.6%	29.6%	0.7219	0.6906	98.8%	0.1711	0.0081	24.457	
	01:38	01:40	2.0	187.53	150.28	76.26	75.74	38.52	42.90	43.05	43.060	28.91	28.91	29.5%	29.5%	0.7219	0.6900	98.8%	0.1729	0.0082	24.451	
	01:40	01:42	2.0	187.66	150.36	76.60	75.68	38.46	42.88	42.99	42.999	27.95	27.95	29.4%	29.4%	0.7219	0.6895	98.8%	0.1745	0.0082	24.446	
	01:42	01:44	2.0	187.53	150.38	76.72	75.26	38.51	42.87	42.92	42.937	27.96	27.96	29.3%	29.3%	0.7219	0.6893	98.8%	0.1754	0.0083	24.455	
	01:44	01:46	2.0	187.73	150.39	77.09	75.15	38.70	42.88	42.96	42.874	28.79	28.79	29.2%	29.2%	0.7219	0.6887	98.8%	0.1753	0.0084	24.453	
	01:46	01:48	2.0	187.71	150.24	76.96	75.06	38.41	42.76	42.80	42.812	27.90	27.90	28.5%	28.5%	0.7219	0.6890	98.8%	0.1763	0.0083	24.444	
	01:48	01:50	2.0	187.80	150.13	77.08	75.10	38.35	42.79	42.74	42.751	27.68	27.68	28.9%	28.9%	0.7219	0.6888	98.8%	0.1767	0.0083	24.440	
	01:50	01:52	2.0	187.81	149.99	76.83	74.93	38.25	42.68	42.691	42.740	27.40	27.40	28.8%	28.8%	0.7219	0.6892	98.8%	0.1748	0.0082	24.440	
	01:52	01:54	2.0	187.69	149.87	76.66	75.48	38.34	42.61	42.62	42.631	27.18	27.18	28.7%	28.7%	0.7219	0.6895	98.8%	0.1743	0.0082	24.445	
	01:54	01:56	2.0	187.96	149.84	76.48	75.12	38.52	42.57	42.56	42.572	26.92	26.92	28.6%	28.6%	0.7219	0.6897	98.8%	0.1741	0.0082	24.435	
	01:56	01:58	2.0	187.86	149.37	76.04	74.70	38.43	42.19	42.52	42.510	27.88	27.88	28.5%	28.5%	0.7219	0.6902	98.8%	0.1728	0.0081	24.436	
	01:58	02:00	2.0	187.69	149.11	76.05	74.01	38.62	42.11	42.48	42.44	42.451	27.00	27.00	28.4%	28.4%	0.7219	0.6901	98.8%	0.1720	0.0081	24.432
	02:00	02:02	2.0	187.87	149.71	76.03	74.87	38.14	42.39	42.38	42.390	27.57	27.57	28.3%	28.3%	0.7219	0.6906	98.9%	0.1703	0.0080	24.438	
	02:02	02:04	2.0	187.95	149.59	76.11	74.85	38.25	42.33	42.32	42.329	27.72	27.72	28.2%	28.2%	0.7219	0.6905	98.9%	0.1700	0.0080	24.438	
	02:04	02:06	2.0	187.86	149.37	76.04	74.70	38.43	42.19	42.25	42.268	27.71	27.71	28.1%	28.1%	0.7219	0.6904	98.8%	0.1713	0.0081	24.438	
	02:06	02:08	2.0	187.69	149.11	76.05	74.65	38.38	42.11	42.20	42.208	27.09	27.09	27.5%	27.5%	0.7219	0.6904	98.8%	0.1707	0.0081	24.445	
	02:08	02:10	2.0	187.71	148.97	75.93	74.62	38.32	42.01	42.13	42.148	27.44	27.44	27.8%	27.8%	0.7219	0.6913	98.9%	0.1699	0.0079	24.462	
	02:10	02:12	2.0	187.40	148.69	75.58	74.71	38.13	41.87	42.08	42.090	26.51	26.51	27.3%	27.3%	0.7219	0.6912	98.9%	0.1672	0.0079	24.465	
	02:12	02:14	2.0	187.50	148.69	75.52	74.68	38.23	41.80	42.02	42.032	26.00	26.00	27.6%	27.6%	0.7219	0.6912	98.9%	0.1677	0.0079	24.452	
	02:14	02:16	2.0	187.29	148.61	75.29	74.41	38.02	41.73	41.96	41.976	25.47	25.47	27.5%	27.5%	0.7219	0.6917	98.9%	0.1656	0.0078	24.460	
	02:16	02:18	2.0	187.22	148.67	75.50	74.56	38.08	41.71	41.91	41.920	25.37	25.37	27.4%	27.4%	0.7219	0.6913	98.9%	0.1671	0.0079	24.462	
	02:18	02:20	2.0	187.15	148.77	75.59	74.49	38.03	41.63	41.85	41.865	25.10	25.10	27.3%	27.3%	0.7219	0.6912	98.9%	0.1672	0.0079	24.465	
	02:20	02:22	2.0	187.74	148.74	75.81	74.33	38.15	41.61	41.80	41.810	25.19	25.19	27.2%	27.2%	0.7219	0.6906	98.9%	0.1688	0.0080	24.465	
	02:22	02:24	2.0	187.35	148.64	75.95	74.91	38.25	41.58	41.74	41.753	25.70	25.70	27.1%	27.1%	0.7219	0.6906	98.9%	0.1701	0.0081	24.465	

TGOC Concentration , Mass Emissions and Emissions Factor											
Cm ft	A F	B G	E	J	I	D	C	H	Mass TGOC lbm-C	Mass Mgas Accum lbm-C	Mass Cgas(Dry) ppmv
VMc dscf	VWc scf	VWW scf	Wood H2 Volume	Inject Air Moisture BWSi	Psycho BWSi %	VWi scf	VMi dscf	Ve wscf	Cgas(wet) ppmv	Cgas(Dry) ppmv	TGOC ppmv
17.31	1.25	1.38	1.06	4.61	21.16	19.52	1665.96	2147.44	88.80	30.36	88.33
25.84	7.12	458.98	1.38	29.15	21.22	0.046	3.998	5.310	78.2	1.3E-05	104.8
19.32	5.20	458.98	1.16	21.22	0.045	3.906	5.278	78.0	1.3E-05	104.5	2.08E-03
18.236	6.203	1.279	1.148	25.382	0.047	4.029	5.390	78.1	1.3E-05	104.7	2.08E-03
18.267	6.185	1.322	1.135	25.294	0.045	3.906	5.278	78.0	1.3E-05	104.5	2.08E-03
18.235	6.211	1.312	1.154	25.406	0.047	4.018	5.355	78.0	1.3E-05	104.5	2.10E-03
18.243	6.203	1.299	1.154	25.373	0.047	4.018	5.355	78.0	1.3E-05	104.5	2.12E-03
18.261	6.193	1.303	1.146	25.324	0.046	3.959	5.307	77.9	1.3E-05	104.3	2.13E-03
18.259	6.196	1.268	1.155	25.338	0.045	3.849	5.177	78.1	1.3E-05	104.6	2.14E-03
18.243	6.197	1.203	1.166	25.355	0.045	3.775	5.019	77.7	1.2E-05	104.2	2.15E-03
18.268	6.176	1.211	1.150	25.267	0.043	3.691	4.938	77.9	1.2E-05	104.2	2.17E-03
18.269	6.182	1.240	1.148	25.282	0.044	3.767	5.060	77.8	1.2E-05	104.1	2.18E-03
18.257	6.185	1.213	1.162	25.304	0.045	3.793	5.048	77.7	1.2E-05	104.1	2.19E-03
18.276	6.169	1.220	1.150	25.235	0.045	3.826	5.084	77.7	1.2E-05	103.9	2.20E-03
18.298	6.153	1.248	1.151	25.166	0.045	3.881	5.177	77.6	1.3E-05	103.8	2.22E-03
18.302	6.145	1.271	1.151	25.135	0.047	4.035	5.357	77.6	1.3E-05	103.6	2.23E-03
18.322	6.122	1.283	1.149	25.044	0.047	4.083	5.411	77.6	1.3E-05	103.5	2.24E-03
18.345	6.101	1.243	1.152	24.958	0.047	4.009	5.300	77.7	1.3E-05	103.5	2.25E-03
18.371	6.075	1.238	1.157	24.850	0.047	3.981	5.261	77.8	1.3E-05	103.5	2.27E-03
18.394	6.056	1.272	1.164	24.768	0.048	4.060	5.375	77.5	1.3E-05	103.1	2.28E-03
18.408	6.047	1.295	1.151	24.727	0.047	4.069	5.415	77.5	1.3E-05	103.0	2.29E-03
18.402	6.049	1.268	1.146	24.740	0.047	4.079	5.388	77.6	1.3E-05	103.0	2.31E-03
18.422	6.035	1.300	1.135	24.676	0.048	4.182	5.532	77.5	1.3E-05	102.9	2.32E-03
18.435	6.021	1.386	1.131	24.620	0.051	4.430	5.869	77.1	1.4E-05	102.3	2.33E-03
18.439	6.014	1.341	1.131	24.595	0.049	4.291	5.681	77.2	1.4E-05	102.4	2.35E-03
18.445	6.008	1.317	1.146	24.571	0.050	4.285	5.578	76.8	1.3E-05	102.3	2.36E-03
18.438	6.005	1.358	1.155	24.497	0.050	4.270	5.667	77.1	1.4E-05	102.1	2.37E-03
18.466	5.991	1.338	1.155	24.497	0.050	4.079	5.388	77.6	1.3E-05	102.1	2.37E-03
18.460	5.991	1.363	1.168	24.503	0.051	4.293	5.711	77.2	1.4E-05	102.3	2.39E-03
18.443	6.003	1.318	1.179	24.554	0.050	4.188	5.551	77.2	1.3E-05	102.3	2.40E-03
18.444	6.007	1.318	1.185	24.566	0.050	4.202	5.619	76.5	1.3E-05	101.8	2.42E-03
18.523	5.922	1.282	1.178	24.227	0.050	4.196	5.538	77.0	1.3E-05	101.6	2.43E-03
18.521	5.914	1.269	1.176	24.202	0.050	4.239	5.557	76.7	1.3E-05	101.1	2.44E-03
18.543	5.893	1.315	1.167	24.116	0.051	4.306	5.676	76.5	1.4E-05	100.9	2.51E-03
18.542	5.890	1.273	1.162	24.109	0.049	4.149	5.465	76.5	1.3E-05	100.9	2.46E-03
18.544	5.894	1.300	1.148	24.119	0.051	4.351	5.705	76.4	1.4E-05	101.0	2.47E-03
18.561	1.307	1.154	24.037	0.052	4.470	5.826	76.4	1.4E-05	100.6	2.48E-03	
18.598	5.840	1.307	1.156	23.898	0.053	4.534	5.888	76.3	1.4E-05	101.1	2.50E-03
18.642	5.802	1.277	1.156	23.737	0.051	4.384	5.713	76.2	1.4E-05	100.9	2.51E-03
18.664	5.780	1.294	1.149	23.646	0.053	4.575	5.910	76.2	1.4E-05	99.9	2.58E-03
18.716	5.740	1.250	1.130	23.470	0.048	4.232	5.534	76.3	1.3E-05	99.8	2.59E-03
18.713	5.739	1.226	1.131	23.471	0.048	4.215	5.482	76.3	1.3E-05	99.7	2.61E-03
18.730	5.729	1.201	1.116	23.423	0.045	4.019	5.263	76.0	1.2E-05	99.2	2.62E-03
18.722	5.741	1.196	1.126	23.467	0.045	3.963	5.202	76.1	1.2E-05	99.5	2.64E-03
18.708	5.783	1.183	1.128	23.534	0.046	4.023	5.255	76.1	1.2E-05	99.5	2.66E-03
18.711	5.751	1.188	1.139	23.511	0.047	4.109	5.349	75.9	1.3E-05	99.2	2.67E-03
18.725	5.733	1.212	1.148	23.439	0.048	4.171	5.431	75.6	1.3E-05	98.7	2.68E-03

		54.94 lbm		Starting Mass		0.9830 Meter (Y)		TGOC analyzer calib Span		84		250.6		227.8 ppmv		19.77 Start Cal Tim		
		26.84 lbm		29.9000 inHg		101.25 kPa		Zero		0		0.38		-3.8 ppmv		22.45 End Cal Tim		
		28.10 lbm		Total Mass Displaced		Load cell calibration		Zero		50		50		50.07 lbm		11.714057 Chamber		
1A	1B	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Interval	Start Time	End Time	Duration	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	"Value"	(A+B) & (F+G)
Start Time	Time	End Time	min	Tc F	Twb F	Tm F	Ambient F	Meter & Meter	Drift M	Corrected M	Wood Wm	Water Wm	Moisture dWw	%Bwc	Wood Reading cuff dVm	Inlet Meter Volume Dry Vm(std)	Inlet Air Fraction dr mfg(inlet) dscf	Vc(x) wscf
Range to 12% H2O	Min	Max	Avg/Sum	124.52	95.77	76.12	73.96	24.46	36.32	33.41	41.68	41.695	26.10	27.0%	0.7219	0.6904	93.9%	0.0080
02:24	02:26	02:28	2.0	187.33	148.57	76.41	74.03	38.09	41.47	41.62	41.638	26.26	26.9%	0.7219	0.6939	93.8%	0.1718	0.0081
02:26	02:28	02:30	2.0	187.53	148.36	76.13	73.93	37.88	41.39	41.57	41.582	25.21	26.8%	0.7219	0.6904	93.9%	0.1694	0.0080
02:30	02:32	02:34	2.0	187.79	148.33	76.27	73.93	37.97	41.37	41.51	41.525	25.87	26.7%	0.7219	0.6902	93.8%	0.1705	0.0080
02:32	02:34	02:36	2.0	187.74	148.24	76.03	73.91	37.74	41.30	41.46	41.470	25.22	26.6%	0.7219	0.6906	93.9%	0.1682	0.0079
02:34	02:36	02:38	2.0	187.63	148.13	76.12	73.66	37.95	41.29	41.40	41.415	24.92	26.5%	0.7219	0.6904	93.9%	0.1696	0.0080
02:36	02:38	02:40	2.0	187.46	147.92	75.82	73.68	38.04	41.20	41.34	41.359	25.28	26.4%	0.7219	0.6908	93.9%	0.1684	0.0079
02:38	02:40	02:42	2.0	187.45	147.83	75.89	73.54	37.96	41.21	41.29	41.303	25.52	26.3%	0.7219	0.6907	93.9%	0.1684	0.0079
02:40	02:42	02:44	2.0	187.47	147.70	75.75	73.70	38.01	41.12	41.23	41.247	25.54	26.2%	0.7219	0.6909	93.9%	0.1679	0.0079
02:42	02:44	02:46	2.0	187.54	147.62	75.85	73.64	38.25	41.08	41.18	41.191	25.03	26.1%	0.7219	0.6907	93.9%	0.1695	0.0080
02:44	02:46	02:48	2.0	187.65	147.53	75.99	73.87	37.87	41.01	41.12	41.136	25.29	26.0%	0.7219	0.6906	93.9%	0.1686	0.0079
02:46	02:48	02:50	2.0	187.78	147.37	76.17	73.40	37.92	41.00	41.07	41.082	24.36	25.9%	0.7219	0.6903	93.9%	0.1698	0.0080
02:48	02:50	02:52	2.0	187.86	147.22	76.07	73.58	38.09	40.91	41.02	41.030	23.84	25.8%	0.7219	0.6904	93.9%	0.1700	0.0080
02:50	02:52	02:54	2.0	187.81	147.14	76.15	73.41	38.09	40.89	40.96	40.977	23.86	25.7%	0.7219	0.6903	93.8%	0.1704	0.0080
02:52	02:54	02:56	2.0	187.68	146.97	76.17	73.30	38.13	40.87	40.91	40.927	22.84	25.6%	0.7219	0.6903	93.8%	0.1707	0.0081
02:54	02:56	02:58	2.0	187.84	146.89	76.15	73.12	37.81	40.84	40.86	40.877	22.40	25.5%	0.7219	0.6904	93.9%	0.1692	0.0080
02:56	02:58	03:00	2.0	187.75	146.81	75.92	73.12	37.68	40.74	40.81	40.829	22.06	25.4%	0.7219	0.6907	93.9%	0.1674	0.0079
02:58	03:00	03:02	2.0	187.77	146.73	76.05	72.93	37.85	40.76	40.81	40.779	22.63	25.3%	0.7219	0.6905	93.9%	0.1688	0.0080
03:00	03:02	03:04	2.0	187.56	146.59	75.92	72.93	37.96	40.64	40.71	40.730	22.38	25.3%	0.7219	0.6907	93.9%	0.1686	0.0079
03:02	03:04	03:06	2.0	187.65	146.52	76.06	73.05	38.10	40.58	40.66	40.679	22.83	25.2%	0.7219	0.6904	93.9%	0.1700	0.0080
03:04	03:06	03:08	2.0	187.59	146.44	76.19	72.88	37.83	40.53	40.61	40.628	23.25	25.1%	0.7219	0.6903	93.9%	0.1695	0.0080
03:06	03:08	03:10	2.0	187.68	146.34	76.35	72.80	37.86	40.52	40.56	40.577	23.30	25.0%	0.7219	0.6900	98.8%	0.1705	0.0080
03:08	03:10	03:12	2.0	187.82	146.33	76.32	72.73	38.17	40.50	40.51	40.526	22.91	24.9%	0.7219	0.6901	98.8%	0.1713	0.0081
03:10	03:12	03:14	2.0	187.97	146.31	76.34	72.85	38.10	40.46	40.46	40.478	22.05	24.8%	0.7219	0.6899	98.8%	0.1728	0.0081
03:12	03:14	03:16	2.0	187.98	146.27	76.39	72.70	38.06	40.41	40.41	40.428	22.54	24.7%	0.7219	0.6899	98.8%	0.1716	0.0081
03:14	03:16	03:18	2.0	187.86	146.12	76.28	72.76	38.01	40.37	40.36	40.380	22.00	24.6%	0.7219	0.6901	98.8%	0.1708	0.0081
03:16	03:18	03:20	2.0	187.80	146.06	76.32	72.73	38.17	40.30	40.32	40.331	22.29	24.5%	0.7219	0.6900	98.8%	0.1717	0.0081
03:18	03:20	03:22	2.0	187.63	145.95	76.43	72.56	38.31	40.23	40.27	40.282	21.95	24.4%	0.7219	0.6898	98.8%	0.1729	0.0082
03:20	03:22	03:24	2.0	187.69	145.81	76.54	72.64	38.17	40.18	40.22	40.232	22.75	24.3%	0.7219	0.6897	98.8%	0.1729	0.0082
03:22	03:24	03:26	2.0	187.77	145.67	76.69	72.54	37.77	40.14	40.17	40.183	22.30	24.3%	0.7219	0.6895	98.8%	0.1719	0.0081
03:24	03:26	03:28	2.0	187.66	145.47	76.68	72.38	37.94	40.06	40.12	40.134	22.35	24.2%	0.7219	0.6895	98.8%	0.1726	0.0081
03:26	03:28	03:30	2.0	187.74	145.33	76.58	72.51	37.94	40.00	40.07	40.086	21.86	24.1%	0.7219	0.6897	98.8%	0.1716	0.0081
03:28	03:30	03:32	2.0	187.69	145.25	76.53	72.33	38.19	39.97	40.02	40.037	22.20	24.0%	0.7219	0.6902	98.8%	0.1707	0.0081
03:30	03:32	03:34	2.0	187.70	145.08	76.32	72.40	38.39	39.87	39.97	39.989	21.56	23.9%	0.7219	0.6903	98.9%	0.1726	0.0081
03:32	03:34	03:36	2.0	187.79	145.03	76.27	72.40	38.16	39.82	39.93	39.941	21.78	23.8%	0.7219	0.6904	98.8%	0.1714	0.0081
03:34	03:36	03:38	2.0	187.81	144.91	76.23	72.18	38.25	39.79	39.88	39.892	22.24	23.7%	0.7219	0.6901	98.8%	0.1711	0.0081
03:36	03:38	03:40	2.0	187.74	144.91	76.23	72.14	38.06	39.75	39.83	39.843	21.37	23.3%	0.7219	0.6906	98.8%	0.1716	0.0081
03:38	03:40	03:42	2.0	187.78	144.75	76.14	71.96	37.95	39.68	39.78	39.796	21.47	23.6%	0.7219	0.6907	98.9%	0.1692	0.0080
03:40	03:42	03:44	2.0	187.79	144.45	76.09	71.72	38.31	39.62	39.73	39.749	21.57	23.5%	0.7219	0.6903	98.9%	0.1703	0.0081
03:42	03:44	03:46	2.0	187.74	144.39	75.94	71.67	38.35	39.49	39.64	39.655	21.35	23.4%	0.7219	0.6904	98.8%	0.1711	0.0081
03:44	03:46	03:48	2.0	187.78	144.22	75.87	71.54	38.15	39.42	39.59	39.607	21.70	23.2%	0.7219	0.6907	98.9%	0.1716	0.0081
03:46	03:48	03:50	2.0	187.37	144.07	75.97	71.39	38.27	39.41	39.54	39.558	22.37	23.1%	0.7219	0.6905	98.9%	0.1703	0.0080
03:48	03:50	03:52	2.0	187.43	143.87	76.05	71.65	38.41	39.41	39.49	39.507	22.78	23.0%	0.7219	0.6904	98.8%	0.1713	0.0081
03:50	03:52	03:54	2.0	187.45	143.71	76.05	71.42	38.47	39.35	39.44	39.456	23.24	22.9%	0.7219	0.6904	98.8%	0.1716	0.0081
03:52	03:54	03:56	2.0	187.60	143.48	76.36	71.35	38.38	39.32	39.39	39.405	23.20	22.8%	0.7219	0.6899	98.8%	0.1728	0.0081
03:54	03:56	03:58	2.0	187.69	143.11	76.57	71.34	38.33	39.29	39.34	39.354	23.42	22.7%	0.7219	0.6896	98.8%	0.1737	0.0082

TGOC Concentration , Mass Emissions and Emissions Factor									
Cm ft ³	A F	B G	E Wood H2 VWW scf	J Inlet Air Moisture BWSi %	I Psycho BWSi %	D VMi dscf	C Ve wsfc	H Cgas(wet) ppmv	G Mass TGOC lbm-C
VMc dscf	VWc scf	VWi scf	VWSc %	VWSc %	VWSc %	VWSc %	VWSc %	VWSc ppmv	VWSc ppmv
17.31	1.25	25.84	7.12	458.98	1.06	4.61	0.049	4.181	5.472
19.32	5.20	19.16	21.22	1.16	29.15	19.52	1665.96	2147.44	75.6
18.736	5.722	1.231	1.148	23.396	0.049	4.181	25.99	20.36	98.6
18.726	5.721	1.238	1.161	23.402	0.052	4.404	5.690	88.80	2.69E-03
18.764	5.687	1.189	1.144	23.261	0.048	4.116	5.363	75.5	1.3E-05
18.763	5.678	1.220	1.151	23.231	0.050	4.263	5.530	75.5	1.3E-05
18.778	5.665	1.189	1.136	23.178	0.048	4.195	5.428	75.5	1.3E-05
18.798	5.649	1.175	1.145	23.106	0.049	4.234	5.451	75.3	1.3E-05
18.834	5.620	1.192	1.137	22.982	0.049	4.230	5.471	75.3	1.3E-05
18.848	5.606	1.204	1.137	22.926	0.050	4.325	5.579	75.2	1.3E-05
18.868	5.585	1.204	1.133	22.840	0.049	4.302	5.558	75.3	1.3E-05
18.879	5.572	1.180	1.144	22.789	0.049	4.241	5.475	75.3	1.3E-05
18.890	5.557	1.192	1.138	22.730	0.050	4.363	5.611	75.5	1.3E-05
18.911	5.530	1.148	1.146	22.625	0.049	4.219	5.420	75.0	1.3E-05
18.932	5.506	1.124	1.148	22.531	0.048	4.100	5.269	75.2	1.2E-05
18.947	5.494	1.125	1.151	22.477	0.049	4.181	5.349	75.1	1.3E-05
18.975	5.470	1.077	1.153	22.378	0.046	3.973	5.102	74.6	2.81E-03
18.984	5.455	1.056	1.142	22.321	0.045	3.893	4.991	74.8	1.3E-05
18.998	5.445	1.040	1.130	22.275	0.044	3.851	4.937	74.8	1.2E-05
19.010	5.432	1.067	1.140	22.224	0.046	4.002	5.108	74.6	1.2E-05
19.035	5.414	1.055	1.138	22.144	0.045	3.928	5.032	74.6	1.3E-05
19.044	5.403	1.076	1.148	22.100	0.047	4.022	5.143	74.7	1.2E-05
19.057	5.392	1.096	1.144	22.053	0.048	4.133	5.280	74.6	1.2E-05
19.070	5.375	1.098	1.151	21.987	0.048	4.080	5.231	74.5	1.2E-05
19.069	5.371	1.080	1.157	21.977	0.047	4.025	5.158	74.6	1.2E-05
19.068	5.366	1.040	1.167	21.961	0.046	3.891	4.977	74.5	1.2E-05
19.074	5.360	1.063	1.159	21.936	0.048	4.070	5.176	74.3	1.2E-05
19.099	5.339	1.038	1.153	21.848	0.046	3.924	5.006	74.5	1.2E-05
19.110	5.331	1.051	1.160	21.811	0.047	4.022	5.114	74.4	1.2E-05
19.130	5.317	1.035	1.168	21.748	0.047	4.007	5.092	74.3	1.2E-05
19.233	5.212	1.047	1.168	21.320	0.049	4.188	5.284	74.1	1.2E-05
19.149	5.296	1.073	1.168	21.664	0.049	4.181	5.304	74.3	1.2E-05
19.258	5.187	1.016	1.166	21.218	0.047	3.989	5.056	74.1	1.2E-05
19.170	5.273	1.051	1.162	21.574	0.049	4.160	5.258	74.3	1.2E-05
19.201	5.246	1.054	1.167	21.458	0.049	4.163	5.269	74.1	1.2E-05
19.220	5.223	1.031	1.162	21.367	0.047	4.033	5.109	74.2	1.2E-05
19.304	5.137	1.013	1.146	21.019	0.047	4.093	5.150	73.7	1.2E-05
19.325	5.119	1.017	1.156	20.942	0.049	4.155	5.214	73.4	1.2E-05
19.353	5.097	1.007	1.155	20.848	0.047	4.042	5.088	73.5	1.2E-05
19.366	5.092	1.008	1.151	20.820	0.048	4.163	5.216	73.4	1.2E-05
19.393	5.067	1.023	1.142	20.717	0.049	4.233	5.309	73.3	1.2E-05
19.412	5.044	1.055	1.149	20.626	0.052	4.433	5.542	73.2	1.3E-05
19.440	5.014	1.074	1.157	20.505	0.053	4.506	5.634	73.4	1.3E-05
19.463	4.991	1.049	1.159	21.116	0.048	4.100	5.196	92.8	3.17E-03
19.492	4.956	1.094	1.167	20.273	0.057	4.854	5.848	92.0	3.23E-03
19.542	4.903	1.104	1.174	20.056	0.058	4.845	6.012	73.1	1.4E-05

Start Time	End Time	measured	Starting Mass			0.9830 Meter (Y)			TGOC analyzer calib Span			84			250.6			227.8 ppmv			19.77 Start-Cal Tim					
			26.84 lbm			29.9000 inHg			Zero			50			0			0.38			-3.8 ppmv			22.45 End Cal Tim		
			28.10 lbm			101.25 kPa			Load cell calibration			50			0			0.08			0.07 lbm			DBFT		
1A	1B	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26
Interval	Interval	Duration	"Value"	Tc	Twb	"Value"	VOC	"Value"	M	Drift	Calculated	Wood	Water	Wood	Wood	Water	Water	Inlet Meter	Inlet Meter	Inlet Water	Volume	Volume	Volume	Volume	(A+B) & (F+G)	Chamber
Start Time	End Time	min		F	F		ppmv		Corrected	Mass	Water	Change	dWw	Moisture	%Bwc	Wma	Wma	Wma	Wma	Wma	Wma	Wma	Wma	Wma	Wma	Wma
03:38	04:00	2.0	187.83	142.88	76.66	71.26	38.61	33.41	33.45	33.47	0.48	38.26	51.1%	0.7219	39.301	23.58	22.6%	0.7219	0.6894	98.8%	0.1755	0.0083	24.440	24.438		
04:00	04:02	2.0	187.87	142.83	76.75	71.08	38.87	39.17	39.23	39.17	0.48	39.18	39.197	22.5%	0.7219	0.6892	0.6893	0.7219	0.6893	98.8%	0.1755	0.0084	24.438	24.438		
04:02	04:04	2.0	187.86	142.76	76.68	71.08	38.89	39.12	39.08	39.13	0.48	39.13	39.146	22.4%	0.7219	0.6895	0.6895	0.7219	0.6895	98.8%	0.1755	0.0083	24.435	24.435		
04:04	04:06	2.0	187.94	142.69	76.56	70.99	39.06	39.08	39.08	39.08	0.48	39.08	39.096	22.3%	0.7219	0.6897	0.6897	0.7219	0.6897	98.8%	0.1753	0.0083	24.435	24.435		
04:06	04:08	2.0	187.96	142.61	76.42	71.07	38.85	39.04	39.04	39.03	0.48	39.03	39.049	22.2%	0.7219	0.6901	0.6901	0.7219	0.6901	98.8%	0.1753	0.0082	24.435	24.435		
04:08	04:10	2.0	187.87	142.54	76.21	71.12	38.60	39.01	39.01	39.03	0.48	39.01	39.049	22.2%	0.7219	0.6901	0.6901	0.7219	0.6901	98.8%	0.1753	0.0082	24.435	24.435		
04:10	04:12	2.0	187.70	142.47	76.15	70.87	38.58	38.97	38.98	39.01	0.48	39.01	39.001	22.1%	0.7219	0.6902	0.6902	0.7219	0.6902	98.8%	0.1752	0.0081	24.435	24.435		
04:12	04:14	2.0	187.64	142.40	76.23	70.83	39.04	38.93	38.95	38.96	0.48	38.95	38.956	22.0%	0.7219	0.6900	0.6900	0.7219	0.6900	98.8%	0.1751	0.0083	24.435	24.435		
04:14	04:16	2.0	187.56	142.33	76.34	70.80	39.19	38.87	38.89	38.910	0.48	38.89	38.910	21.9%	0.7219	0.6898	0.6898	0.7219	0.6898	98.8%	0.1751	0.0083	24.435	24.435		
04:16	04:18	2.0	187.50	142.26	76.37	70.71	38.98	38.84	38.85	38.864	0.48	38.85	38.864	21.8%	0.7219	0.6898	0.6898	0.7219	0.6898	98.8%	0.1751	0.0083	24.435	24.435		
04:18	04:20	2.0	187.53	142.19	76.52	70.62	39.17	38.81	38.80	38.817	0.48	38.80	38.817	21.8%	0.7219	0.6895	0.6895	0.7219	0.6895	98.8%	0.1751	0.0083	24.435	24.435		
04:20	04:22	2.0	187.55	142.12	76.49	70.71	39.38	38.76	38.75	38.770	0.48	38.76	38.770	21.7%	0.7219	0.6895	0.6895	0.7219	0.6895	98.8%	0.1751	0.0083	24.435	24.435		
04:22	04:24	2.0	187.51	142.05	76.34	70.43	39.26	38.72	38.71	38.724	0.48	38.72	38.724	21.6%	0.7219	0.6898	0.6898	0.7219	0.6898	98.8%	0.1751	0.0083	24.435	24.435		
04:24	04:26	2.0	187.59	141.98	76.14	70.73	39.01	38.66	38.66	38.679	0.48	38.66	38.679	21.5%	0.7219	0.6901	0.6901	0.7219	0.6901	98.8%	0.1751	0.0083	24.435	24.435		
04:26	04:28	2.0	187.50	141.91	75.99	70.40	39.34	38.58	38.62	38.634	0.48	38.62	38.634	21.4%	0.7219	0.6903	0.6903	0.7219	0.6903	98.8%	0.1751	0.0083	24.435	24.435		
04:28	04:30	2.0	187.53	141.84	76.09	70.29	39.31	38.51	38.57	38.590	0.48	38.51	38.590	21.4%	0.7219	0.6901	0.6901	0.7219	0.6901	98.8%	0.1751	0.0083	24.435	24.435		
04:30	04:32	2.0	187.59	141.77	76.21	70.47	39.19	38.45	38.53	38.545	0.48	38.45	38.545	21.3%	0.7219	0.6900	0.6900	0.7219	0.6900	98.8%	0.1751	0.0083	24.435	24.435		
04:32	04:34	2.0	187.59	141.70	76.32	70.60	39.28	38.38	38.48	38.501	0.48	38.38	38.501	21.2%	0.7219	0.6898	0.6898	0.7219	0.6898	98.8%	0.1751	0.0083	24.435	24.435		
04:34	04:36	2.0	187.59	141.63	76.35	70.39	39.36	38.33	38.44	38.457	0.48	38.33	38.457	21.1%	0.7219	0.6897	0.6897	0.7219	0.6897	98.8%	0.1751	0.0083	24.435	24.435		
04:36	04:38	2.0	187.52	141.56	76.38	70.07	39.35	38.27	38.40	38.413	0.48	38.27	38.413	21.0%	0.7219	0.6897	0.6897	0.7219	0.6897	98.8%	0.1751	0.0083	24.435	24.435		
04:38	04:40	2.0	187.49	141.49	76.15	70.20	39.23	38.16	38.35	38.370	0.48	38.16	38.370	20.9%	0.7219	0.6901	0.6901	0.7219	0.6901	98.8%	0.1751	0.0083	24.435	24.435		
04:40	04:42	2.0	187.48	141.42	75.94	70.18	39.20	38.11	38.31	38.326	0.48	38.11	38.326	20.8%	0.7219	0.6904	0.6904	0.7219	0.6904	98.8%	0.1751	0.0083	24.435	24.435		
04:42	04:44	2.0	187.38	141.35	75.73	69.94	39.13	38.08	38.26	38.282	0.48	38.08	38.282	20.7%	0.7219	0.6898	0.6898	0.7219	0.6898	98.8%	0.1751	0.0083	24.435	24.435		
04:44	04:46	2.0	187.39	141.31	75.63	69.64	39.17	38.06	38.22	38.236	0.48	38.06	38.236	20.7%	0.7219	0.6907	0.6907	0.7219	0.6907	98.8%	0.1751	0.0083	24.435	24.435		
04:46	04:48	2.0	187.43	141.22	75.67	69.51	39.14	38.03	38.17	38.190	0.48	38.03	38.190	20.6%	0.7219	0.6908	0.6908	0.7219	0.6908	98.8%	0.1751	0.0083	24.435	24.435		
04:48	04:50	2.0	187.54	141.15	75.65	69.57	39.05	38.05	38.13	38.144	0.48	38.05	38.144	20.5%	0.7219	0.6909	0.6909	0.7219	0.6909	98.8%	0.1751	0.0083	24.435	24.435		
04:50	04:52	2.0	187.56	141.08	75.63	69.48	38.90	38.04	38.08	38.099	0.48	38.04	38.099	20.5%	0.7219	0.6909	0.6909	0.7219	0.6909	98.8%	0.1751	0.0083	24.435	24.435		
04:52	04:54	2.0	187.57	141.01	75.77	69.39	38.98	38.02	38.04	38.054	0.48	38.02	38.054	20.4%	0.7219	0.6907	0.6907	0.7219	0.6907	98.8%	0.1751	0.0083	24.435	24.435		
04:54	04:56	2.0	187.57	140.94	75.83	69.23	38.84	37.96	37.99	37.99	0.48	37.99	37.99	20.3%	0.7219	0.6907	0.6907	0.7219	0.6907	98.8%	0.1751	0.0083	24.435	24.435		
04:56	04:58	2.0	187.57	140.88	75.77	69.17	38.76	37.66	37.73	37.749	0.48	37.66	37.749	20.2%	0.7219	0.6908	0.6908	0.7219	0.6908	98.8%	0.1751	0.0083	24.435	24.435		
04:58	05:00	2.0	187.62	140.81	75.67	69.18	38.55	37.55	37.53	37.548	0.48	37.55	37.548	20.1%	0.7219	0.6910	0.6910	0.7219	0.6910	98.8%	0.1751	0.0083	24.435	24.435		
05:00	05:02	2.0	187.65	140.74	75.82	69.18	38.65	37.79	37.86	37.880	0.48	37.79	37.880	20.1%	0.7219	0.6907	0.6907	0.7219	0.6907	98.8%	0.1751	0.0083	24.435	24.435		
05:02	05:04	2.0	187.68	140.68	75.84	68.92	38.88	37.74	37.82	37.836	0.48	37.82	37.836	20.0%	0.7219	0.6906	0.6906	0.7219	0.6906	98.8%	0.1751	0.0083	24.435	24.435		
05:04	05:06	2.0	187.71	140.61	75.91	68.72	40.00	37.60	37.61	37.626	0.48	37.60	37.626	19.9%	0.7219	0.6904	0.6904	0.7219	0.6904	98.8%	0.1751	0.0083	24.435	24.435		
05:06	05:08	2.0	187.																							

TGOC Concentration , Mass Emissions and Emissions Factor											
A F	B G	C H	D I	E J	F K	G L	H M	I N	J O	K P	L Q
VMc dscf	VWc scf	WoodH2 VWW scf	Inlet Air Moisture BWSi %	Psycho BWSi %	VWi scf	VMi dscf	Ve wsfc	Cgas(wet) ppmv	Mass TGOC Mgas lbm-C	Mass TGOC Mgas lbm-C	Mass TGOC Mgas lbm-C
17.31	1.25	1.06	4.61					25.99	30.36		
25.84	7.12	1.38	29.15					88.80	118.40		
19.32	5.20	458.98	1.16	21.22	19.32	1665.96	2147.44	68.61	88.33		
19.572	4.867	1.123	1.186	19.915	0.057	4.789	5.971	73.0	1.4E-05	91.2	3.22E-03
19.578	4.860	1.112	1.198	19.888	0.058	4.776	5.945	72.9	1.4E-05	90.9	3.29E-03
19.588	4.850	1.105	1.196	19.846	0.058	4.764	5.930	72.9	1.3E-05	90.9	3.30E-03
19.597	4.839	1.095	1.196	19.803	0.057	4.731	5.884	72.8	1.3E-05	90.8	3.32E-03
19.606	4.828	1.067	1.184	19.761	0.055	4.618	5.737	72.9	1.3E-05	90.8	3.33E-03
19.618	4.820	1.024	1.169	19.722	0.052	4.437	5.507	72.9	1.3E-05	90.8	3.34E-03
19.632	4.812	1.011	1.165	19.686	0.052	4.396	5.457	72.7	1.2E-05	90.5	3.35E-03
19.644	4.803	0.975	1.183	19.647	0.051	4.252	5.275	72.6	1.2E-05	90.4	3.37E-03
19.655	4.794	0.977	1.191	19.609	0.052	4.276	5.303	72.6	1.2E-05	90.3	3.38E-03
19.667	4.785	0.994	1.186	19.570	0.052	4.364	5.412	72.5	1.2E-05	90.2	3.39E-03
19.676	4.775	1.007	1.198	19.528	0.054	4.436	5.497	72.4	1.2E-05	90.0	3.40E-03
19.685	4.765	0.996	1.203	19.487	0.054	4.394	5.441	72.5	1.2E-05	90.1	3.41E-03
19.696	4.755	0.985	1.194	19.448	0.053	4.362	5.402	72.3	1.2E-05	89.7	3.43E-03
19.704	4.744	0.978	1.178	19.406	0.052	4.344	5.378	72.6	1.2E-05	90.0	3.44E-03
19.711	4.733	0.964	1.182	19.363	0.051	4.280	5.289	72.2	1.2E-05	89.6	3.45E-03
19.725	4.726	0.938	1.185	19.328	0.050	4.187	5.177	72.1	1.2E-05	89.4	3.46E-03
19.733	4.715	0.951	1.186	19.287	0.051	4.258	5.263	72.3	1.2E-05	89.6	3.47E-03
19.740	4.704	0.951	1.193	19.245	0.052	4.266	5.268	72.5	1.2E-05	89.7	3.48E-03
19.750	4.695	0.942	1.197	19.206	0.051	4.229	5.216	72.2	1.2E-05	89.4	3.49E-03
19.764	4.688	0.933	1.198	19.171	0.051	4.208	5.190	71.9	1.2E-05	89.0	3.51E-03
19.774	4.679	0.935	1.185	19.133	0.051	4.224	5.209	72.1	1.2E-05	89.1	3.52E-03
19.784	4.669	0.931	1.176	19.095	0.050	4.214	5.192	72.0	1.2E-05	89.0	3.53E-03
19.795	4.661	0.955	1.166	19.060	0.051	4.334	5.341	71.8	1.2E-05	88.7	3.54E-03
19.804	4.652	0.976	1.163	19.021	0.052	4.439	5.469	71.5	1.2E-05	88.3	3.56E-03
19.813	4.642	0.987	1.164	18.981	0.053	4.506	5.551	71.4	1.2E-05	88.1	3.57E-03
19.820	4.631	0.985	1.160	18.940	0.053	4.504	5.543	71.4	1.2E-05	88.1	3.58E-03
19.828	4.621	0.967	1.155	18.901	0.052	4.433	5.452	71.4	1.2E-05	88.0	3.59E-03
19.838	4.612	0.956	1.163	18.863	0.052	4.395	5.403	71.3	1.2E-05	87.8	3.61E-03
19.847	4.603	0.945	1.161	18.825	0.051	4.357	5.354	71.1	1.2E-05	87.6	3.62E-03
19.856	4.593	0.920	1.155	18.787	0.050	4.254	5.225	71.1	1.2E-05	87.6	3.63E-03
19.864	4.584	0.919	1.146	18.749	0.049	4.203	5.227	71.1	1.2E-05	87.3	3.64E-03
19.872	4.574	0.940	1.155	18.711	0.051	4.365	5.358	71.1	1.2E-05	87.1	3.65E-03
19.881	4.564	0.947	1.162	18.672	0.052	4.411	5.412	70.8	1.2E-05	87.1	3.66E-03
19.889	4.555	0.945	1.178	18.635	0.053	4.421	5.422	71.0	1.2E-05	87.3	3.67E-03
19.896	4.545	0.917	1.215	18.596	0.053	4.303	5.272	71.1	1.2E-05	86.6	3.68E-03
19.906	4.536	0.896	1.201	18.560	0.051	4.210	5.154	70.9	1.1E-05	86.3	3.69E-03
19.916	4.529	0.876	1.201	18.526	0.050	4.134	5.062	70.7	1.1E-05	86.1	3.70E-03
19.924	4.519	0.869	1.204	18.488	0.050	4.109	5.028	70.6	1.1E-05	86.7	3.71E-03
19.933	4.510	0.841	1.196	18.452	0.048	3.987	4.877	70.6	1.1E-05	86.6	3.72E-03
19.942	4.501	0.821	1.188	18.415	0.047	3.908	4.781	70.4	1.0E-05	86.3	3.73E-03
19.948	4.491	0.786	1.185	18.376	0.045	3.752	4.586	70.3	1.0E-05	86.1	3.74E-03
19.955	4.481	0.757	1.185	18.338	0.043	3.621	4.422	70.1	9.7E-06	85.9	3.75E-03
19.963	4.472	0.733	1.183	18.301	0.042	3.514	4.287	69.9	9.3E-06	85.6	3.76E-03
19.973	4.464	0.668	1.178	18.267	0.038	3.215	3.921	70.2	8.6E-06	85.8	3.78E-03
19.982	4.456	0.655	1.180	18.233	0.038	3.156	3.843	70.3	8.4E-06	85.9	3.79E-03
19.994	4.449	0.672	1.186	18.202	0.039	3.246	3.954	70.1	8.6E-06	85.6	3.80E-03
20.004	4.442	0.687	1.191	18.169	0.040	3.323	4.046	69.8	8.8E-06	85.3	3.81E-03

Northwest Hardwood Alder 19-Jan-99 mevndrb												54.94 lbm 26.84 lbm 28.10 lbm		Starting Mass Ending Mass Total Mass Displaced		0.9830 Meter (Y) 29.9000 inHg 101.25 kPa		TGOC analyzer calib Span Zero		84 0 50 50 50.12 lbm		227.8 ppmv -3.8 ppmv 50.12 lbm		19.77 Start-Cal Tim 22.45 End Cal Tim 11.714057	
1A	1B	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	(A+B) & (F+G)	Chamber 30.01					
Range to 12% H ₂ O	Interval Start Time	Interval End Time	Duration min	"Value" T _c F	"Value" T _b F	"Value" T _m F	"Value" Ambient & Meter	"Value" RH %	"Value" VOC ppmv	"Value" W/m lbm	Corrected Mass W/m lbm	Wood Water Change dW/W gm	Moisture % Bwc	Volume Vm(wet) ft ³	Inlet Meter Reading cuff dVm ft ³	Volume Vm(std) dscf	Inlet Air Fraction dry mg(inlet)	Inlet Water Change gm	Inlet Water Volume Vw(std) dscf	Vc(x) wscf					
Min	Max	Avg/Sum	938	124.52	95.77	67.45	24.46	36.32	33.41	33.45	33.47	0.48	12.0%	51.1%	329.25	31.47	81.47	3.84	24.52						
05.32	05.34	2.0	187.57	139.70	76.26	67.75	39.40	37.15	37.27	37.284	14.83	19.0%	0.7219	0.6899	98.8%	0.1769	0.1769	0.0083	24.449						
05.34	05.36	2.0	187.66	139.63	76.20	67.72	39.17	37.13	37.23	37.250	15.22	18.9%	0.7219	0.6900	98.8%	0.1755	0.1755	0.0083	24.446						
05.36	05.38	2.0	187.72	139.57	75.82	67.62	38.80	37.12	37.20	37.217	15.12	18.9%	0.7219	0.6907	98.8%	0.1718	0.1718	0.0081	24.444						
05.38	05.40	2.0	187.70	139.51	75.76	67.52	38.75	37.09	37.17	37.184	15.00	18.8%	0.7219	0.6908	98.8%	0.1712	0.1712	0.0081	24.444						
05.40	05.42	2.0	187.80	139.44	75.79	67.39	38.53	37.02	37.13	37.151	15.12	18.7%	0.7219	0.6908	98.8%	0.1704	0.1704	0.0080	24.441						
05.42	05.44	2.0	187.83	139.38	75.66	67.41	38.53	36.96	37.10	37.117	15.19	18.7%	0.7219	0.6910	98.9%	0.1698	0.1698	0.0080	24.						
05.44	05.46	2.0	187.81	139.32	75.53	67.45	38.49	36.92	37.06	37.083	15.79	18.6%	0.7219	0.6912	98.9%	0.1689	0.1689	0.0080	24.44~						
05.46	05.48	2.0	187.66	139.25	75.69	67.15	38.36	36.91	37.03	37.046	16.36	18.5%	0.7219	0.6910	98.9%	0.1692	0.1692	0.0080	24.446						
05.48	05.50	2.0	187.69	139.19	75.84	67.03	38.26	36.88	36.99	37.009	16.75	18.5%	0.7219	0.6907	98.9%	0.1695	0.1695	0.0080	24.445						
05.50	05.52	2.0	187.57	139.13	75.82	67.04	38.27	36.84	36.95	36.973	16.69	18.4%	0.7219	0.6908	98.9%	0.1695	0.1695	0.0080	24.449						
05.52	05.54	2.0	187.56	139.07	75.81	66.99	38.27	36.80	36.92	36.936	16.52	18.3%	0.7219	0.6908	98.9%	0.1694	0.1694	0.0080	24.450						
05.54	05.56	2.0	187.52	139.01	75.87	66.85	38.35	36.78	36.88	36.900	16.30	18.3%	0.7219	0.6907	98.9%	0.1701	0.1701	0.0080	24.451						
05.56	05.58	2.0	187.57	138.94	75.86	67.04	38.18	36.77	36.85	36.865	15.91	18.2%	0.7219	0.6907	98.9%	0.1693	0.1693	0.0080	24.449						
05.58	06.00	2.0	187.66	138.88	75.92	66.80	37.97	36.77	36.81	36.831	15.64	18.1%	0.7219	0.6907	98.9%	0.1687	0.1687	0.0080	24.446						
06.00	06.02	2.0	187.78	138.82	75.95	66.48	37.87	36.72	36.78	36.797	15.17	18.1%	0.7219	0.6907	98.9%	0.1684	0.1684	0.0079	24.441						
06.02	06.04	2.0	187.84	138.76	75.99	66.25	37.81	36.72	36.75	36.766	14.42	18.0%	0.7219	0.6906	98.9%	0.1683	0.1683	0.0079	24.439						
06.04	06.06	2.0	187.91	138.70	76.08	66.46	38.01	36.81	36.72	36.737	13.21	18.0%	0.7219	0.6904	98.9%	0.1697	0.1697	0.0080	24.436						
06.06	06.08	2.0	187.88	138.64	76.26	66.42	38.13	36.81	36.69	36.710	12.13	17.9%	0.7219	0.6901	98.8%	0.1712	0.1712	0.0081	24.437						
06.08	06.10	2.0	187.76	138.58	76.13	66.13	37.95	36.75	36.66	36.684	11.76	17.9%	0.7219	0.6904	98.9%	0.1697	0.1697	0.0080	24.435						
06.10	06.12	2.0	187.96	138.52	75.92	66.26	38.02	36.74	36.64	36.657	12.37	17.8%	0.7219	0.6907	98.9%	0.1689	0.1689	0.0080	24.435						
06.12	06.14	2.0	187.95	138.46	75.96	66.23	37.88	36.71	36.61	36.628	12.92	17.8%	0.7219	0.6906	98.9%	0.1685	0.1685	0.0079	24.435						
06.14	06.16	2.0	187.90	138.40	76.23	66.20	38.24	36.65	36.58	36.598	13.83	17.7%	0.7219	0.6904	98.9%	0.1715	0.1715	0.0081	24.437						
06.16	06.18	2.0	187.88	138.34	76.29	65.95	38.03	36.61	36.55	36.567	14.17	17.7%	0.7219	0.6901	98.8%	0.1709	0.1709	0.0081	24.437						
06.18	06.20	2.0	187.76	138.28	76.20	65.93	37.89	36.55	36.52	36.535	14.52	17.6%	0.7219	0.6903	98.9%	0.1697	0.1697	0.0080	24.442						
06.20	06.22	2.0	187.57	138.22	76.21	66.04	37.57	36.47	36.48	36.503	14.35	17.6%	0.7219	0.6907	98.9%	0.1689	0.1689	0.0079	24.449						
06.22	06.24	2.0	187.45	138.16	76.09	65.89	37.93	36.43	36.45	36.473	13.93	17.5%	0.7219	0.6904	98.9%	0.1694	0.1694	0.0080	24.454						
06.24	06.26	2.0	187.43	138.10	75.78	65.62	38.03	36.33	36.42	36.444	13.04	17.4%	0.7219	0.6909	98.9%	0.1682	0.1682	0.0079	24.453						
06.26	06.28	2.0	187.44	138.04	75.54	65.67	37.84	36.22	36.39	36.414	13.41	17.4%	0.7219	0.6913	98.9%	0.1661	0.1661	0.0078	24.453						
06.28	06.30	2.0	187.44	137.98	75.49	65.61	37.84	36.16	36.36	36.383	14.19	17.3%	0.7219	0.6914	98.9%	0.1659	0.1659	0.0078	24.454						
06.30	06.32	2.0	187.38	137.92	75.55	65.51	37.73	36.14	36.33	36.351	14.51	17.3%	0.7219	0.6903	98.9%	0.1656	0.1656	0.0078	24.456						
06.32	06.34	2.0	187.48	137.86	75.78	65.47	37.68	36.12	36.30	36.318	14.85	17.2%	0.7219	0.6910	98.9%	0.1666	0.1666	0.0079	24.453						
06.34	06.36	2.0	187.47	137.81	75.88	65.48	37.90	36.14	36.27	36.285	15.14	17.2%	0.7219	0.6908	98.9%	0.1682	0.1682	0.0079	24.453						
06.36	06.38	2.0	187.46	137.75	75.88	65.50	37.88	36.13	36.23	36.252	15.27	17.1%	0.7219	0.6908	98.9%	0.1675	0.1675	0.0079	24.453						
06.38	06.40	2.0	187.61	137.69	76.00	65.06	38.04	36.15	36.20	36.218	15.02	17.0%	0.7219	0.6906	98.9%	0.1694	0.1694	0.0080	24.448						
06.40	06.42	2.0	187.66	137.63	76.12	65.18	37.68	36.15	36.17	36.185	15.01	17.0%	0.7219	0.6904	98.9%	0.1684	0.1684	0.0079	24.446						
06.42	06.44	2.0	187.57	137.55	75.87	64.66	38.15	36.06	36.13	36.154	14.24	16.9%	0.7219	0.6905	98.9%	0.1679	0.1679	0.0079	24.444						
06.44	06.46	2.0	187.70	137.52	76.00	64.83	37.61	36.17	36.12	36.145	14.45	16.9%	0.7219	0.6906	98.9%	0.1675	0.1675	0.0079	24.444						
06.46	06.48	2.0	187.70	137.46	76.05	64.86	37.57	36.18	36.07	36.088	15.61	16.8%	0.7219	0.6912	98.9%	0.1676	0.1676	0.0079	24.445						
06.48	06.50	2.0	187.62	137.40	76.03	64.76	38.03	36.15	36.03	36.052	16.12	16.7%	0.7219	0.6905	98.9%	0.1656	0.1656	0.0078	24.453						
06.50	06.52	2.0	187.57	137.35	75.87	64.66	37.68	36.12	36.08	36.018	15.80	16.7%	0.7219	0.6907	98.9%	0.1667	0.1667	0.0079	24.452						
06.52	06.54	2.0	187.46	137.29	75.75	64.49	37.70	36.01	35.96	35.983	15.92	16.6%	0.7219	0.6910	98.9%	0.1666	0.1666	0.0079	24.453						
06.54	06.56	2.0	187.41	137.23	75.73	64.37	37.62	35.91	35.93	35.947	16.19	16.5%	0.7219	0.6911	98.9%	0.1661	0.1661	0.0078	24.455						
06.56	06.58	2.0	187.47	137.18	75.61	64.63	37.65	35.87	35.89	35.911	16.20	16.5%	0.7219	0.6912	98.9%	0.1656	0.1656	0.0078	24.453						
06.58	07.00	2.0	187.49	137.12	75.65	64.32	37.85	35.83	35.86	35.876	16.03	16.4%	0.7219	0.6911	98.9%	0.1667	0.1667	0.0079	24.452						
07.00	07.02	2.0	187.57	137.07	75.56	64.42	37.88	35.81	35.82	35.841	15.74	16.3%	0.7219	0.6913	98.9%	0.1664	0.1664	0.0078	24.452						
07.02	07.04	2.0	187.68	137.01	75.63	64.30	37.84	35.78	35.79	35.809	14.85	16.3%	0.7219	0.6912	98.9%	0.1665	0.1665	0.0078	24.453						
07.04	07.06	2.0	187.70	136.96	75.81	64.15	37.47	35.80	35.77	35.777	14.32	16.2%	0.7219	0.6910	98.9%	0.1665	0.1665	0.0078	24.453						

Cm ft	A F	B G	E VWc scf	J Wood H2 Volume VWW scf	I Inlet Air Moisture BWSi %	D Psycho BWSc %	C VMi dscf	H Ve wsfc	G Cgas(wet) ppmv	TGOC Mass TGOC Ibm-C	F Mgas ppmv	G Cgas(Dry) ppmv	H Mgas Accum Ibm-C	I Emission Factor EF	J Emission Factor EF	K Emission Factor EF	L Emission Factor Accum Ibm/Mdbit
20.015	4.434	0.699	1.194	18.137	0.041	3.401	4.145	69.7	9.0E-06	85.1	3.82E-03	7.7E-04	0.3257				
20.021	4.425	0.718	1.185	18.099	0.042	3.495	4.257	69.7	9.0E-06	85.1	3.82E-03	7.9E-04	0.3265				
20.028	4.415	0.713	1.160	18.063	0.041	3.472	4.225	69.6	9.2E-06	84.9	3.83E-03	7.8E-04	0.3273				
20.037	4.407	0.707	1.155	18.029	0.040	3.460	4.211	69.5	9.1E-06	84.8	3.84E-03	7.8E-04	0.3281				
20.043	4.397	0.713	1.150	17.992	0.041	3.492	4.246	69.4	9.2E-06	84.6	3.85E-03	7.8E-04	0.3288				
20.051	4.389	0.716	1.145	17.957	0.041	3.512	4.268	69.4	9.2E-06	84.6	3.86E-03	7.9E-04	0.3296				
20.060	4.381	0.745	1.139	17.923	0.042	3.649	4.430	69.4	9.6E-06	84.6	3.87E-03	8.2E-04	0.3304				
20.072	4.374	0.781	1.141	17.894	0.044	3.853	4.669	69.1	1.0E-05	84.2	3.88E-03	8.6E-04	0.3313				
20.079	4.366	0.790	1.144	17.859	0.045	3.889	4.719	69.0	1.0E-05	84.0	3.89E-03	8.7E-04	0.3322				
20.090	4.359	0.787	1.143	17.829	0.045	3.888	4.719	69.0	1.0E-05	84.0	3.90E-03	8.7E-04	0.3330				
20.099	4.351	0.779	1.143	17.796	0.045	3.857	4.680	69.0	1.0E-05	83.9	3.91E-03	8.6E-04	0.3339				
20.108	4.343	0.769	1.148	17.764	0.044	3.821	4.636	68.8	9.9E-06	83.7	3.92E-03	8.5E-04	0.3347				
20.115	4.335	0.750	1.142	17.729	0.043	3.740	4.537	69.0	9.8E-06	83.9	3.93E-03	8.3E-04	0.3356				
20.121	4.325	0.737	1.138	17.694	0.042	3.688	4.473	68.8	9.6E-06	83.6	3.94E-03	8.2E-04	0.3364				
20.126	4.316	0.715	1.136	17.657	0.041	3.584	4.342	68.5	9.3E-06	83.1	3.95E-03	7.9E-04	0.3372				
20.132	4.307	0.680	1.136	17.622	0.039	3.420	4.142	68.2	8.9E-06	82.8	3.96E-03	7.5E-04	0.3379				
20.139	4.298	0.623	1.146	17.587	0.036	3.141	3.799	68.5	9.1E-06	83.1	3.97E-03	6.9E-04	0.3386				
20.147	4.290	0.572	1.156	17.556	0.034	2.900	3.509	68.4	7.5E-06	83.0	3.97E-03	6.4E-04	0.3393				
20.154	4.281	0.554	1.146	17.521	0.033	2.816	3.403	68.1	7.2E-06	82.6	3.98E-03	6.2E-04	0.3399				
20.161	4.273	0.583	1.140	17.489	0.034	2.963	3.580	68.3	7.6E-06	82.7	3.99E-03	6.5E-04	0.3405				
20.170	4.266	0.609	1.137	17.457	0.036	3.099	3.743	68.2	8.0E-06	82.7	4.00E-03	6.8E-04	0.3412				
20.178	4.258	0.652	1.158	17.426	0.039	3.326	4.017	68.2	8.5E-06	82.6	4.01E-03	7.3E-04	0.3419				
20.187	4.251	0.668	1.154	17.395	0.040	3.407	4.110	68.0	7.5E-06	82.3	4.01E-03	7.4E-04	0.3427				
20.197	4.245	0.684	1.146	17.367	0.040	3.492	4.210	67.9	8.9E-06	82.2	4.02E-03	7.6E-04	0.3435				
20.209	4.240	0.677	1.137	17.341	0.040	3.461	4.173	68.1	8.9E-06	82.3	4.03E-03	7.6E-04	0.3442				
20.220	4.234	0.657	1.144	17.314	0.039	3.375	4.070	67.9	8.6E-06	82.1	4.04E-03	7.4E-04	0.3449				
20.228	4.226	0.615	1.135	17.283	0.036	3.169	3.821	67.6	8.1E-06	81.8	4.05E-03	6.9E-04	0.3456				
20.236	4.219	0.633	1.120	17.251	0.037	3.262	3.932	67.7	8.3E-06	81.8	4.06E-03	7.1E-04	0.3463				
20.243	4.211	0.669	1.119	17.221	0.039	3.454	4.160	67.7	8.8E-06	81.7	4.07E-03	7.5E-04	0.3471				
20.252	4.204	0.684	1.117	17.191	0.040	3.546	4.274	67.6	9.0E-06	81.6	4.07E-03	7.7E-04	0.3479				
20.257	4.195	0.700	1.124	17.157	0.041	3.631	4.371	67.5	9.2E-06	81.5	4.08E-03	7.9E-04	0.3486				
20.265	4.155	0.671	1.134	16.999	0.040	3.527	4.239	67.0	8.5E-06	80.8	4.13E-03	7.6E-04	0.3494				
20.296	4.148	0.681	1.130	16.968	0.041	3.712	4.468	67.5	9.4E-06	81.5	4.10E-03	8.1E-04	0.3503				
20.273	4.181	0.720	1.134	17.097	0.043	3.759	4.528	67.5	9.5E-06	80.6	4.14E-03	7.7E-04	0.3517				
20.277	4.171	0.708	1.143	17.062	0.043	3.706	4.459	67.1	9.3E-06	80.9	4.11E-03	8.0E-04	0.3511				
20.283	4.163	0.708	1.137	17.030	0.043	3.709	4.461	67.2	9.3E-06	81.0	4.12E-03	8.0E-04	0.3519				
20.289	4.155	0.671	1.134	16.999	0.040	3.584	4.306	67.0	8.5E-06	80.8	4.13E-03	8.4E-04	0.3559				
20.331	4.122	0.751	1.124	16.857	0.045	3.973	4.767	66.6	9.9E-06	80.1	4.18E-03	8.4E-04	0.3567				
20.340	4.116	0.763	1.121	16.830	0.046	4.054	4.865	66.4	1.0E-05	79.9	4.19E-03	8.6E-04	0.3576				
20.345	4.108	0.764	1.117	16.799	0.046	4.063	4.874	66.7	1.0E-05	80.2	4.20E-03	8.7E-04	0.3585				
20.352	4.100	0.756	1.125	16.769	0.046	4.035	4.840	66.4	1.0E-05	79.8	4.21E-03	8.6E-04	0.3593				
20.357	4.128	0.745	1.142	16.883	0.045	3.936	4.722	66.7	9.8E-06	80.3	4.17E-03	8.4E-04	0.3602				
20.362	4.084	0.700	1.122	16.737	0.045	3.972	4.764	66.5	9.9E-06	79.9	4.22E-03	8.4E-04	0.3610				
20.368	4.076	0.675	1.119	16.676	0.041	3.629	4.346	66.2	9.0E-06	79.5	4.24E-03	7.7E-04	0.3617				

Cm ft	A F	B G	E	J	D	C	H	TGOC Concentration , Mass Emissions and Emissions Factor						
VMc dscf	VWc scf	Wood H2 VWW scf	Inlet Air Volume BWSc scf	Moisture Psycho BWSc %	VWi scf	VMi dscf	Ve wsfc	Cgas(wet) ppmv	Mass TGOC Mgas lbm-C	Mass TGOC Mgas ppmv	Mass Accum Ibm-C	Emission Factor EF	Emission Factor EF	Emission Factor EF Accum lbm/Mdbit
17.31	1.25	4.069	1.06	4.61				25.99		30.36				
25.84	7.12	458.98	1.38	29.15	21.22	19.52	1665.96	2147.44	88.80	118.40	88.33			0.40
19.32	5.20		1.16											
20.375	4.069	4.621	1.135	16.647	0.039	3.336	4.018	66.2	8.3E-06	79.5	4.25E-03	7.1E-04	0.3624	
20.380	4.061	0.580	1.122	16.616	0.036	3.131	3.742	66.2	7.7E-06	79.4	4.25E-03	6.6E-04	0.3631	
20.389	4.055	0.555	1.112	16.590	0.034	3.026	3.627	66.1	7.5E-06	79.2	4.26E-03	6.4E-04	0.3637	
20.388	4.044	0.565	1.108	16.552	0.035	3.104	3.728	66.0	7.7E-06	79.1	4.27E-03	6.6E-04	0.3644	
20.380	4.028	0.556	1.089	16.504	0.034	3.068	3.685	65.8	7.6E-06	78.8	4.28E-03	6.5E-04	0.3650	
20.369	4.011	0.570	1.069	16.453	0.034	3.147	3.773	65.6	7.7E-06	78.5	4.28E-03	6.6E-04	0.3657	
20.361	3.996	0.574	1.073	16.406	0.035	3.186	3.822	65.2	7.8E-06	78.0	4.29E-03	6.6E-04	0.3664	
20.351	3.979	0.623	1.078	16.356	0.038	3.458	4.140	64.8	8.4E-06	77.5	4.30E-03	7.1E-04	0.3671	
20.345	3.965	0.659	1.093	16.311	0.040	3.650	4.338	64.6	8.8E-06	77.2	4.31E-03	7.5E-04	0.3678	
20.346	3.955	0.701	1.095	16.276	0.043	3.878	4.624	64.5	9.3E-06	77.0	4.32E-03	7.9E-04	0.3686	
20.351	3.948	0.726	1.092	16.247	0.044	4.020	4.791	64.1	9.6E-06	76.6	4.33E-03	8.2E-04	0.3694	
20.357	3.941	0.760	1.086	16.219	0.046	4.213	5.019	63.8	1.0E-05	76.2	4.34E-03	8.5E-04	0.3703	
20.364	3.935	0.736	1.083	16.192	0.045	4.096	4.879	63.8	9.7E-06	76.2	4.35E-03	8.3E-04	0.3711	
20.370	3.927	0.686	1.086	16.163	0.042	3.821	4.546	63.5	9.0E-06	75.7	4.36E-03	7.7E-04	0.3719	
20.378	3.922	0.682	1.076	16.139	0.041	3.810	4.536	63.4	9.0E-06	75.6	4.37E-03	7.7E-04	0.3726	
20.383	3.914	0.661	1.076	16.111	0.040	3.712	4.423	63.4	8.7E-06	75.5	4.37E-03	7.5E-04	0.3734	
20.384	3.905	0.631	1.085	16.076	0.039	3.553	4.229	63.2	8.3E-06	75.3	4.38E-03	7.1E-04	0.3741	
20.386	3.896	0.595	1.085	16.045	0.037	3.362	3.999	63.1	7.9E-06	75.2	4.39E-03	6.7E-04	0.3748	
20.389	3.887	0.600	1.091	16.013	0.038	3.404	4.050	62.8	7.9E-06	74.8	4.40E-03	6.8E-04	0.3754	
20.390	3.878	0.586	1.083	15.980	0.037	3.331	3.960	62.7	7.7E-06	74.7	4.41E-03	6.6E-04	0.3761	
20.392	3.869	0.608	1.094	15.948	0.038	3.446	4.059	62.6	8.0E-06	74.5	4.41E-03	6.8E-04	0.3768	
20.400	3.864	0.593	1.105	15.924	0.038	3.373	4.001	62.4	7.8E-06	74.2	4.42E-03	6.6E-04	0.3775	
20.408	3.859	0.573	1.105	15.901	0.036	3.267	3.875	62.3	7.5E-06	74.0	4.43E-03	6.4E-04	0.3781	
20.415	3.853	0.538	1.097	15.876	0.035	3.186	3.778	62.2	7.3E-06	73.9	4.44E-03	6.2E-04	0.3787	
20.423	3.847	0.538	1.101	15.852	0.034	3.079	3.649	62.0	7.0E-06	73.7	4.44E-03	6.0E-04	0.3793	
20.431	3.842	0.511	10.983	15.829	0.033	2.936	3.479	60.9	6.6E-06	72.3	4.45E-03	5.6E-04	0.3799	
20.438	3.836	0.509	1.100	15.804	0.033	2.958	3.518	59.5	6.5E-06	70.6	4.46E-03	5.6E-04	0.3804	
20.432	3.824	0.533	1.104	15.763	0.035	3.106	3.693	57.8	7.7E-06	68.6	4.46E-03	5.7E-04	0.3810	
20.425	3.810	0.559	1.100	15.721	0.036	3.265	3.878	56.1	6.8E-06	66.6	4.47E-03	5.8E-04	0.3816	
20.420	3.797	0.582	1.098	15.681	0.038	3.403	4.039	54.6	6.9E-06	64.7	4.48E-03	5.9E-04	0.3822	
20.416	3.786	0.589	1.106	15.642	0.039	3.459	4.105	53.1	6.8E-06	63.0	4.48E-03	5.8E-04	0.3828	
20.410	3.773	0.590	1.104	15.601	0.039	3.452	4.085	51.9	6.6E-06	61.5	4.49E-03	5.6E-04	0.3833	
20.413	3.765	0.577	1.095	15.573	0.037	3.379	3.996	50.8	6.3E-06	60.2	4.50E-03	5.4E-04	0.3839	
20.418	3.759	0.576	1.109	15.546	0.038	3.376	3.988	49.8	6.2E-06	59.0	4.50E-03	5.3E-04	0.3844	
20.425	3.753	0.578	1.110	15.523	0.038	3.408	4.030	48.6	6.1E-06	57.5	4.51E-03	5.2E-04	0.3849	
20.427	3.745	0.558	1.104	15.494	0.037	3.306	3.911	47.5	5.8E-06	56.2	4.51E-03	4.9E-04	0.3854	
20.426	3.736	0.519	1.096	15.461	0.034	3.090	3.656	46.6	5.3E-06	55.2	4.52E-03	4.5E-04	0.3857	
20.430	3.692	0.469	1.115	15.307	0.032	2.814	3.316	42.4	4.4E-06	50.0	4.54E-03	4.3E-04	0.3863	
20.424	3.725	0.509	1.100	15.426	0.034	3.033	3.586	45.2	5.1E-06	53.4	4.53E-03	4.3E-04	0.3863	
20.424	3.716	0.478	1.100	15.393	0.032	2.861	3.382	44.4	4.7E-06	52.5	4.53E-03	4.0E-04	0.3867	
20.423	3.706	0.479	1.103	15.360	0.032	2.870	3.387	43.7	4.6E-06	51.7	4.53E-03	3.9E-04	0.3871	
20.424	3.698	0.464	1.113	15.331	0.031	2.779	3.274	43.2	4.4E-06	51.1	4.54E-03	3.8E-04	0.3875	
20.430	3.692	0.469	1.122	15.206	0.033	2.949	3.470	40.3	4.4E-06	50.0	4.54E-03	3.7E-04	0.3878	
20.435	3.686	0.456	1.116	15.228	0.031	2.747	3.238	41.8	4.2E-06	49.3	4.55E-03	3.6E-04	0.3882	
20.437	3.679	0.469	1.119	15.255	0.032	2.824	3.325	41.4	4.3E-06	48.8	4.55E-03	3.7E-04	0.3886	
20.443	3.673	0.464	1.118	15.231	0.032	2.805	3.302	40.9	4.2E-06	48.2	4.56E-03	3.6E-04	0.3889	
20.447	3.667	0.488	1.122	15.206	0.033	2.949	3.470	40.3	4.4E-06	47.5	4.56E-03	3.7E-04	0.3893	
20.453	3.661	0.515	1.121	15.183	0.035	3.116	3.666	39.8	4.6E-06	46.9	4.56E-03	3.9E-04	0.3897	

Northwest Hardwood

		54.94 lbm		Starting Mass		0.9830 Meter (Y)		TGOC analyzer calib Span		84		250.6		227.8 ppmv		19.77 Start Cal Tim	
		26.84 lbm		Ending Mass		29.9000 inHg 101.25 kPa		Zero		50		50		-3.8 ppmv		22.45 End Cal Tim	
		28.10 lbm		Total Mass Displaced				Load cell calibration		0		0		0.08		0.07 lbm	
LA	1B	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
Interval	Start Time	End Time	Duration	"Value"	"Value"	"Value"	"Value"	"Value"	Drift	Calculated	Wood	Wood	Meter	Inlet Meter	Inlet Water	Inlet Water	DBFT
Start Time	Interval	Duration	min	Tc F	Twb F	Tm F	Ambient	& Meter	Corrected Mass Wm	Mass Wm	Water Change dWw	Moisture %Bwc	Volume dVm	Volume dVm(Std)	Volume Vw(Std)	Volume Vw(Std)	Chamber 30.01
Range to 12% H2O	Min	Max	Avg/Sum	124.52	95.77	67.45	24.46	36.32	33.41	33.45	33.47	0.48	12.0%	0	0	0	(A+B) & (F+G)
08:42	08:44	08:46	08:48	196.59	156.96	77.09	87.94	53.13	54.90	54.90	54.91	38.26	51.1%	0	0.08	0.07 lbm	24.11
08:44	08:46	08:48	08:48	196.54	134.42	74.30	36.94	39.89	34.34	34.42	34.44	10.78	13.8%	0.8824	0.8469	98.9%	24.113
08:48	08:50	08:52	08:52	196.52	134.38	74.22	36.56	39.86	34.31	34.40	34.42	10.34	13.8%	0.8824	0.8471	98.9%	24.115
08:50	08:52	08:54	08:54	196.43	134.33	74.08	36.03	39.90	34.30	34.38	34.39	9.88	13.7%	0.8824	0.8473	98.9%	24.116
08:52	08:54	08:56	08:56	196.43	134.28	74.03	35.80	40.22	34.28	34.36	34.37	9.20	13.7%	0.8824	0.8473	98.9%	24.117
08:54	08:56	08:58	08:58	196.32	134.24	73.95	35.29	40.32	34.25	34.33	34.35	9.83	13.6%	0.8824	0.8475	98.9%	24.123
08:56	08:58	09:00	09:00	196.30	134.19	73.80	34.77	40.09	34.22	34.31	34.33	10.33	13.6%	0.8824	0.8478	98.9%	24.124
09:00	09:02	09:02	09:02	196.26	134.15	73.71	34.52	40.34	34.21	34.29	34.31	9.74	13.6%	0.8824	0.8479	98.9%	24.126
09:02	09:04	09:04	09:04	196.27	134.10	73.82	34.13	40.06	34.22	34.27	34.29	9.41	13.5%	0.8824	0.8478	98.9%	24.125
09:04	09:06	09:06	09:06	196.24	134.06	73.67	33.99	39.89	34.21	34.25	34.27	9.44	13.5%	0.8824	0.8481	98.9%	24.126
09:06	09:08	09:08	09:08	196.14	134.01	73.66	34.26	39.84	34.24	34.23	34.25	10.02	13.4%	0.8824	0.8481	98.9%	24.130
09:08	09:10	09:10	09:10	196.16	133.97	73.64	34.28	39.88	34.24	34.20	34.22	9.55	13.4%	0.8824	0.8482	98.9%	24.129
09:10	09:12	09:12	09:12	196.12	133.92	73.72	34.01	39.79	34.27	34.18	34.20	9.85	13.4%	0.8824	0.8480	98.9%	24.131
09:12	09:14	09:14	09:14	196.14	133.88	73.69	33.83	39.98	34.27	34.16	34.18	10.08	13.3%	0.8824	0.8480	98.9%	24.129
09:14	09:16	09:16	09:16	196.36	133.79	73.59	33.06	39.97	34.22	34.12	34.14	10.32	13.3%	0.8824	0.8481	98.9%	24.123
09:16	09:18	09:18	09:18	196.37	133.75	73.48	32.89	40.00	34.20	34.19	34.20	10.20	13.2%	0.8824	0.8482	98.9%	24.122
09:18	09:20	09:20	09:20	196.29	133.71	73.31	32.16	40.23	34.15	34.15	34.17	10.34	13.2%	0.8824	0.8484	98.9%	24.121
09:20	09:22	09:22	09:22	196.27	133.66	72.98	31.45	40.34	34.09	34.07	34.09	10.46	13.2%	0.8824	0.8481	98.9%	24.124
09:22	09:24	09:24	09:24	196.15	133.62	72.65	30.71	40.99	34.02	34.03	34.05	9.54	13.1%	0.8824	0.8493	98.9%	24.125
09:24	09:26	09:26	09:26	196.04	133.58	72.31	29.94	41.38	33.99	34.01	34.03	10.20	13.2%	0.8824	0.8498	98.9%	24.129
09:26	09:28	09:28	09:28	196.02	133.54	71.99	29.48	41.56	33.94	33.99	34.00	9.73	13.0%	0.8824	0.8504	98.9%	24.133
09:28	09:30	09:30	09:30	196.12	133.49	71.73	29.05	42.18	33.91	33.97	33.99	9.01	13.0%	0.8824	0.8509	98.9%	24.130
09:30	09:32	09:32	09:32	196.25	133.84	73.68	33.60	39.99	34.26	34.14	34.16	10.32	13.3%	0.8824	0.8493	98.9%	24.123
09:32	09:34	09:34	09:34	196.20	133.45	71.67	28.73	42.66	33.92	33.94	33.96	9.30	12.9%	0.8824	0.8498	98.9%	24.126
09:34	09:36	09:36	09:36	196.20	133.41	71.75	28.62	42.77	33.92	33.94	33.96	9.95	12.9%	0.8824	0.8511	98.9%	24.128
09:36	09:38	09:38	09:38	196.26	133.33	71.78	28.27	43.87	33.90	33.92	33.94	9.73	12.7%	0.8824	0.8504	98.9%	24.133
09:38	09:40	09:40	09:40	196.20	133.29	71.81	27.58	43.11	33.85	33.88	33.90	9.55	12.8%	0.8824	0.8510	98.9%	24.131
09:40	09:42	09:42	09:42	196.09	133.25	71.67	27.21	43.29	33.82	33.84	33.86	9.73	12.8%	0.8824	0.8513	98.9%	24.126
09:42	09:44	09:44	09:44	196.15	133.20	71.40	26.73	43.69	33.83	33.88	33.90	9.55	12.7%	0.8824	0.8511	98.9%	24.127
09:44	09:46	09:46	09:46	196.11	133.16	71.08	26.29	44.13	33.81	33.79	33.81	10.44	12.7%	0.8824	0.8516	98.9%	24.128
09:46	09:48	09:48	09:48	195.99	133.12	70.84	25.88	45.58	33.82	33.88	33.97	11.17	12.6%	0.8824	0.8510	98.9%	24.130
09:48	09:50	09:50	09:50	195.98	133.08	70.60	25.39	44.76	33.79	33.74	33.76	11.22	12.6%	0.8824	0.8513	98.9%	24.126
09:50	09:52	09:52	09:52	196.02	133.04	70.46	25.12	44.96	33.75	33.72	33.74	11.95	12.5%	0.8824	0.8511	98.9%	24.132
09:52	09:54	09:54	09:54	196.04	133.00	70.40	24.84	45.43	33.58	33.69	33.71	12.11	12.5%	0.8824	0.8516	98.9%	24.129
09:54	09:56	09:56	09:56	196.01	132.98	70.62	24.71	45.40	33.65	33.66	33.68	11.69	12.2%	0.8824	0.8532	98.9%	24.134
09:56	09:58	09:58	09:58	196.17	132.92	70.77	24.46	45.36	33.60	33.63	33.65	12.33	12.4%	0.8824	0.8527	98.9%	24.131
09:58	10:00	10:00	10:00	196.33	132.88	70.80	24.50	45.16	33.56	33.61	33.63	12.27	12.3%	0.8824	0.8529	98.9%	24.129
10:00	10:02	10:02	10:02	196.51	132.84	70.92	24.51	45.34	33.60	33.58	33.60	12.15	12.3%	0.8824	0.8531	98.9%	24.134
10:02	10:04	10:04	10:04	196.50	132.80	71.11	24.48	45.02	33.60	33.55	33.58	11.69	12.2%	0.8824	0.8522	98.9%	24.134
10:04	10:06	10:06	10:06	196.48	132.77	71.24	24.60	45.08	33.55	33.53	33.56	10.78	12.2%	0.8824	0.8519	98.9%	24.135
10:06	10:08	10:08	10:08	196.53	132.73	71.40	24.84	44.91	33.55	33.54	33.57	10.12	12.1%	0.8824	0.8513	98.8%	24.116
10:08	10:10	10:10	10:10	196.50	132.69	71.60	24.85	44.83	33.54	33.49	33.52	9.73	12.1%	0.8824	0.8510	98.8%	24.117
10:10	10:12	10:12	10:12	196.54	132.65	71.69	24.91	45.38	33.48	33.47	33.49	9.48	12.1%	0.8824	0.8507	98.8%	24.115
10:12	10:14	10:14	10:14	196.52	132.61	71.59	25.10	53.13	33.41	33.45	33.47	9.55	12.0%	0.8824	0.8491	98.6%	24.116

Crn Fv	TGOC Concentration , Mass Emissions and Emissions Factor											
	A F	B G	C H	D I	E J	F K	G L	H M	I N	J O	K P	L Q
VMc dscf	VWc scf	Wood H2 Volume VWW	Inlet Air Moisture BWSi	VWi scf	Psycho BWSi	VMi dscf	Ve wsfc	Cgas(wet) ppmv	TGOC Mass Mgas lbm-C	Mgas Accum ppmv	TGOC Mass Mgas lbm-C	Emission Factor EF
17.31	1.25	1.06	4.61	3.297	25.99	2147.44	88.80	30.36	4.57E-03	4.11E-04	0.3901	0.3905
25.84	7.12	1.38	29.15	19.52	1665.96	68.61	88.33					0.40
19.32	5.20	458.98	1.16	21.22								
20.458	3.655	0.544	1.128	15.159	0.038	3.129	3.678	39.2	4.55E-06	46.1	4.57E-03	3.81E-04
20.463	3.650	0.515	1.127	15.136	0.036	3.094	3.638	38.6	4.45E-06	45.5	4.58E-03	3.71E-04
20.470	3.645	0.508	1.133	15.115	0.035	2.970	3.489	38.3	4.25E-06	45.1	4.58E-03	3.65E-04
20.476	3.640	0.488	1.129	15.093	0.034	2.849	3.347	37.7	3.95E-06	44.4	4.59E-03	3.48E-04
20.484	3.636	0.466	1.125	15.073	0.032	2.655	3.115	37.5	3.65E-06	44.1	4.59E-03	3.11E-04
20.489	3.630	0.434	1.132	15.051	0.030	2.742	3.214	35.7	3.65E-06	41.9	4.61E-03	0.3918
20.497	3.626	0.464	1.132	15.032	0.033	2.844	3.339	37.0	3.8E-06	43.5	4.59E-03	3.31E-04
20.503	3.621	0.487	1.120	15.010	0.034	2.987	3.506	36.4	4.05E-06	42.9	4.60E-03	3.48E-04
20.509	3.616	0.459	1.123	14.989	0.032	2.828	3.320	36.2	3.75E-06	42.6	3.21E-04	0.3928
20.514	3.611	0.444	1.120	14.967	0.031	2.735	3.209	35.8	3.65E-06	42.1	4.61E-03	3.11E-04
20.520	3.606	0.445	1.109	14.946	0.031	2.742	3.214	35.7	3.65E-06	41.9	4.61E-03	3.03E-04
20.528	3.602	0.473	1.103	14.927	0.033	2.921	3.427	35.9	3.88E-06	42.2	4.61E-03	3.31E-04
20.533	3.596	0.450	1.108	14.905	0.031	2.785	3.265	36.0	3.75E-06	42.3	4.62E-03	3.11E-04
20.539	3.592	0.465	1.108	14.885	0.032	2.883	3.381	35.7	3.85E-06	41.9	4.62E-03	3.21E-04
20.543	3.586	0.475	1.112	14.862	0.033	2.959	3.471	35.5	3.85E-06	41.7	4.62E-03	3.31E-04
20.546	3.580	0.487	1.112	14.837	0.034	3.036	3.561	35.3	3.95E-06	41.4	4.63E-03	3.03E-04
20.549	3.573	0.481	1.109	14.812	0.034	3.000	3.515	34.7	3.85E-06	40.8	4.63E-03	3.21E-04
20.553	3.568	0.488	1.105	14.791	0.034	3.039	3.557	34.6	3.85E-06	40.6	4.64E-03	3.31E-04
20.560	3.564	0.493	1.105	14.773	0.034	3.082	3.609	33.8	3.85E-06	39.7	4.64E-03	3.21E-04
20.566	3.559	0.466	1.096	14.752	0.032	2.913	3.408	33.1	3.55E-06	38.8	4.64E-03	3.31E-04
20.574	3.555	0.450	1.101	14.735	0.031	2.816	3.294	32.3	3.35E-06	37.9	4.65E-03	3.31E-04
20.582	3.552	0.459	1.099	14.718	0.032	2.883	3.373	31.6	3.35E-06	37.0	4.65E-03	3.31E-04
20.587	3.547	0.438	1.095	14.698	0.031	2.763	3.235	31.1	3.15E-06	36.4	4.65E-03	2.75E-04
20.589	3.541	0.425	1.099	14.674	0.030	2.687	3.144	30.6	3.05E-06	35.9	4.66E-03	2.65E-04
20.593	3.535	0.438	1.109	14.651	0.031	2.773	3.242	30.3	3.15E-06	35.5	4.66E-03	3.05E-04
20.597	3.530	0.469	1.115	14.631	0.034	2.976	3.482	30.2	3.35E-06	35.4	4.66E-03	2.85E-04
20.600	3.524	0.456	1.119	14.608	0.033	2.895	3.353	29.9	3.15E-06	35.0	4.67E-03	2.75E-04
20.606	3.520	0.451	1.129	14.589	0.033	2.865	3.347	29.4	3.15E-06	34.5	4.67E-03	2.65E-04
20.611	3.515	0.459	1.126	14.570	0.033	2.914	3.401	29.2	3.15E-06	34.1	4.67E-03	2.65E-04
20.619	3.512	0.458	1.109	14.551	0.031	2.773	3.242	30.3	3.15E-06	35.5	4.66E-03	2.65E-04
20.623	3.507	0.489	1.125	14.532	0.035	3.117	3.640	28.3	3.25E-06	33.1	4.68E-03	2.75E-04
20.628	3.502	0.493	1.124	14.514	0.036	3.141	3.665	27.8	3.25E-06	32.6	4.68E-03	2.75E-04
20.636	3.499	0.527	1.127	14.498	0.038	3.371	3.936	27.4	3.45E-06	32.1	4.68E-03	2.95E-04
20.641	3.495	0.529	1.122	14.479	0.038	3.392	3.960	26.9	3.35E-06	31.5	4.69E-03	2.85E-04
20.645	3.490	0.564	1.122	14.459	0.041	3.615	4.473	28.8	3.15E-06	33.7	4.67E-03	2.75E-04
20.652	3.485	0.571	1.131	14.439	0.042	3.668	4.280	28.3	3.25E-06	33.1	4.68E-03	2.85E-04
20.654	3.480	0.588	1.139	14.421	0.044	3.796	4.433	26.2	3.65E-06	30.7	4.70E-03	3.15E-04
20.666	3.451	0.508	1.155	14.327	0.039	3.371	3.936	26.0	3.65E-06	30.4	4.70E-03	3.05E-04
20.669	3.446	0.477	1.157	14.291	0.036	3.755	4.384	26.0	3.65E-06	30.4	4.71E-03	3.05E-04
20.674	3.442	0.459	1.162	14.274	0.035	3.004	3.500	26.4	2.9E-06	30.8	4.72E-03	2.5E-04
20.678	3.437	0.447	1.175	14.254	0.035	2.992	3.413	26.5	2.8E-06	30.9	4.72E-03	2.4E-04
20.682	3.433	0.451	1.377	14.236	0.042	3.005	3.499	26.7	2.9E-06	31.1	4.73E-03	2.5E-04

Northwest Hardwood
January 19 & 20, 1999

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NOMENCLATURE

- $V_{MC}(x)$: DRY GAS VOLUME OF KILN @ TIME (x) (scf)
 $V_{WC}(x)$: WATER VAPOR VOLUME OF KILN @ TIME (x) (scf)
 $V_{MI}(x)$: DRY GAS VOLUME INLET @ TIME (x) (scf)
 $V_{WI}(x)$: WATER VAPOR VOLUME INLET @ TIME (x) (scf)
 $V_{WW}(x)$: WATER VAPOR VOLUME FROM WOOD @ TIME (x) (scf)
 $V_{MC}(x+1)$: DRY GAS VOLUME OF KILN @ TIME (x+1)
 $V_{WC}(x+1)$: WATER VAPOR VOLUME OF KILN @ TIME (x+1)
 $V_e(x)$: VOLUME OF DRY & WATER VAPOR EXHAUSTING

MEASURED PARAMETERS

T_c : TEMPERATURE; KILN ($^{\circ}$ F) DRY BULB

T_{wb} : " ; KILN ($^{\circ}$ F) WET BULB

T_m : " ; AMBIENT AIR ($^{\circ}$ F)

VOC : PPMV-C WET

RH% : RELATIVE HUMIDITY INLET AIR

M : MASS OF WOOD SAMPLE

CALIBRATIONS

M : VOC ARE DRIFT CORRECTED.

OTHER

SAMPLE TESTED 11.71 DBFT ALDER
 $P_b = 29.90 \text{ inHg}$

EQUATION NO. 1

$$VW_{C(x)} VM_{C(x)} + VW_{C(x)} + VM_{i(x)} + VW_{i(x)} = VM_{c(x+1)} + VW_{c(x+1)} + Vec(x)$$

EQUATION NO. 2

$$\begin{aligned} BWS_{C(x+1)} &= \frac{100 (VW_{C(x)} + VW_{W(x)} + VW_{i(x)})}{VM_{C(x)} + VW_{C(x)} + VW_{W(x)} + VM_{i(x)} + VW_{i(x)}} \\ &= \frac{100 VW_{C(x+1)}}{VM_{C(x+1)} + VW_{C(x+1)}} \end{aligned}$$

KNOWNS

$$VM_{C(x)} = VOL_c \left(\frac{T_{STD} P_c}{T_c P_{STD}} \right) \left(1 - \frac{BWS_{C(x)}}{100} \right)$$

$$VW_{C(x)} = VOL_c \left(\frac{T_{STD} P_c}{T_c P_{STD}} \right) \frac{BWS_{C(x)}}{100}$$

$$* VOL_c = 30.987 - \frac{DBFT}{12}$$

KILN MOISTURE $BWS_{C(x)} = \frac{100 VW_{C(x)}}{VW_{C(x)} + VM_{C(x)}} ;$ FROM PSYCHOMETRY

INLET AIR MOISTURE $BWS_i(x) = \frac{100 VW_{i(x)}}{VW_{i(x)} + VM_{i(x)}} ;$ FROM RH% & INLET TEMPERATURE

* AS THE VOLUME OF INLET AIR INCREASES, THE INITIAL VOLUME OF KILN BECOMES LESS IMPORTANT.

$VM_c(x) \rightarrow A (F)$

$VW_c(x) \rightarrow B (G)$

$VWW(x) \rightarrow E$

$BWS_L \rightarrow J$

$BWS_{C(x+1)} \rightarrow I$

$VW_i(x) \rightarrow D$

$VM_i(x) \rightarrow C$

$VE(x) \rightarrow H$

EQUATION NO. 1

$$A + B + C + D = F + G + H$$

EQUATION NO. 2

$$I = \frac{100(B+E+D)}{(A+B+E+D+C)}$$

SOLVING

$$H ; \quad H = \left(\frac{A+B+C+D}{F+G} \right) = \left(\frac{A+B + \frac{100D}{J}}{F+G} \right)$$

$$J = \frac{100D}{C+D}$$

$$C+D = \frac{100D}{J} \quad C = \frac{100D}{J} - D$$

$$D = \frac{JC}{100-J} \quad C = D \left(\frac{100-J}{J} \right)$$

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$$I = \frac{100(B+E+D)}{A+B+E+D + D\left(\frac{100-I}{J}\right)}$$

SOLVE FOR "D"

(1) $IA + IB + IE + ID + ID\left(\frac{100-I}{J}\right) = 100B + 100E + 100D$

(2) A $IA + IB + IE - 100B - 100E = 100D - ID - ID\left(\frac{100-I}{J}\right)$

(2) B $= D\left(100 - I - I\left(\frac{100-I}{J}\right)\right)$

(2) C $= D\left(\frac{100J - IJ - I(100-I)}{J}\right)$

(2) D $I(A+B+E) - 100(B+E) = D\left[100\left(\frac{J-I}{J}\right)\right]$

(3) $D = \left[I(A+B+E) - 100(B+E)\right] \left[\frac{J}{100(J-I)}\right]$

EQUATION NO I

$$A+B+C+D+E = F+G+H$$

$$C+D = \frac{100D}{J}$$

$$D = \left[\frac{I(A+B+E) - 100(B+E)}{100(J-I)} \right] \left[\frac{J}{100(J-I)} \right]$$

$$C+D = \left(\frac{100}{J} \right) \left(\frac{I(A+B+E) - 100(B+E)}{100(J-I)} \right) \left(\frac{J}{100(J-I)} \right)$$

$$C+D = \left[\frac{I(A+B+E) - 100(B+E)}{(J-I)} \right]$$

$$H = (A+B) - (F+G) + E + \left(\frac{I(A+B+E) - 100(B+E)}{(J-I)} \right)$$

$$V_C(x) = V_{C(x)} - V_{C(x+1)} + V_{WW(x)} + \left[\frac{BWS_{C(x+1)}(V_{C(x)} + V_{WW(x)}) - 100(V_{WW(x)} + V_{WW(x+1)})}{(BWS_{C(x)} - BWS_{C(x+1)})} \right]$$

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$$\frac{BWS_i V_c(x) + BWS_{c(x+1)} VW_{c(x)}}{(BWS_i - BWS_{c(x+1)})} = V_c(x)$$

EXAMPLE CALC.

(I) $\underline{V_c(x)} = 30.01 \left(\frac{527.67}{29.92} \right) \left(\frac{29.90}{174.41 + 459.67} \right) = \underline{24.956}$

$$BWS_c(x) = 20.448 = \frac{100 V_{Wc}(x)}{VM_c(x) + VW_c(x)} = \frac{100 V_{Wc}(x)}{24.956}$$

(II) $\underline{V_{Wc}(x)} = \frac{(20.448)(24.956)}{100} = \underline{5.103}$

(III) $\underline{VM_c(x)} = 24.956 - 5.103 = \underline{19.853}$

(IV) MASS LOSS FOR INTERVAL = 11.23 gm-WATER

$$\underline{VWW(x)} = \frac{(11.23)(0.04707)}{0.99823} = \underline{0.5295}$$

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$$BWS_{C(x+1)} = \left[A - \frac{(P_a - A)(T_{db} - T_{wb})}{2800 - (1.3 T_{wb})} \right] \frac{100}{P_a}$$

$$P_a = 29.90 \text{ inHg}$$

$$T_{db} = 174.42^\circ F$$

$$T_{wb} = 143.78^\circ F$$

$$A = 6.08674 e^{-6} T_{wb}^3 - 1.00431 e^{-3} T_{wb}^2 + 7.56026 e^{-2} T_{wb} - 1.69343$$

$$A = 6.08674 e^{-6} (143.78)^3 = 18.091734$$

$$- 1.00431 e^{-3} (143.78)^2 = - 20.761788$$

$$+ 7.56026 e^{-2} (143.78) = 10.870142$$

$$- 1.69343 = - 1.69343$$

$$6.50666$$

$$\underline{BWS_{C(x+1)}} = \frac{6.50666 - (29.90 - 6.50666)(174.42 - 143.78)}{(2800 - (1.3 \times 143.78))}$$

$$29.90$$

$$= 100 \left[\frac{6.50666 - \left(\frac{716.772}{2613.086} \right)}{29.90} \right] = 20.844$$

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INLET AIR MOISTURE

$$BWS_i(x) = \frac{RH\% \exp}{P_a} \left(18.6866 - 0.00243724 T_a - \frac{4509.47}{T_a} - \frac{149541}{T_a^2} \right)$$

$$RH\% = 48.1$$

$$T_a = 71.35 ^\circ F$$

$$P_a = 29.90 \text{ in Hg}$$

$$(T_a) = 71.35 ^\circ F = \left(\frac{71.35 - 32.2}{1.8} \right) + 273.15 = 294.9 K$$

$$(P_a) = 29.90 \text{ in Hg} = 101.325 \left(\frac{29.90}{29.92126} \right)$$

$$(P_a) = 101.253$$

$$\left(18.6866 - 0.00243724(294.9) - \frac{4509.47}{294.9} - \frac{149541}{(294.9)^2} \right)$$

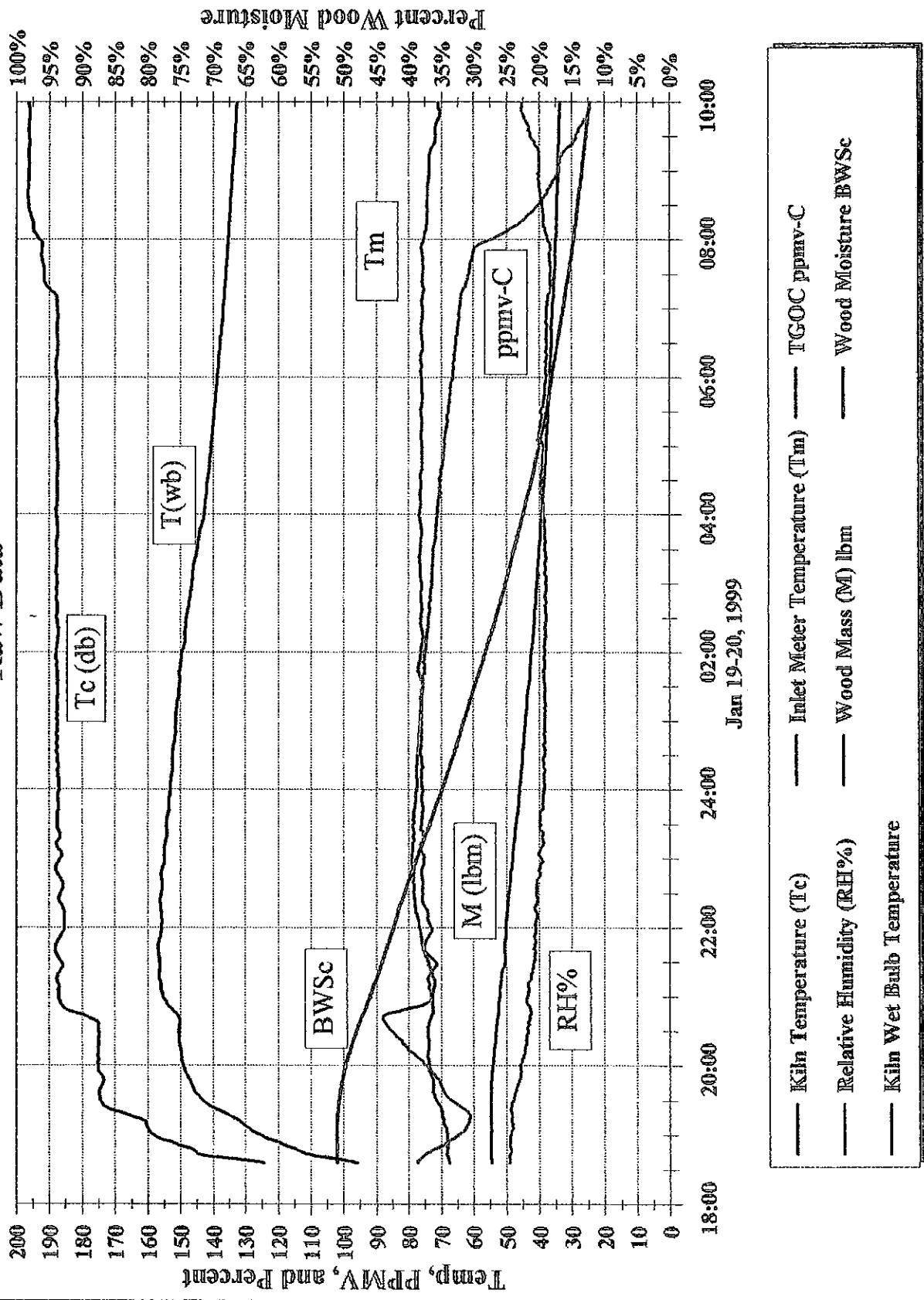
$$BWS_i(x) = \left(\frac{48.1}{101.253} \right) \exp$$

$$(0.9568015)$$

(V) $BWS_i(x) = \frac{48.1 \exp}{101.253} = 1.237 \%$

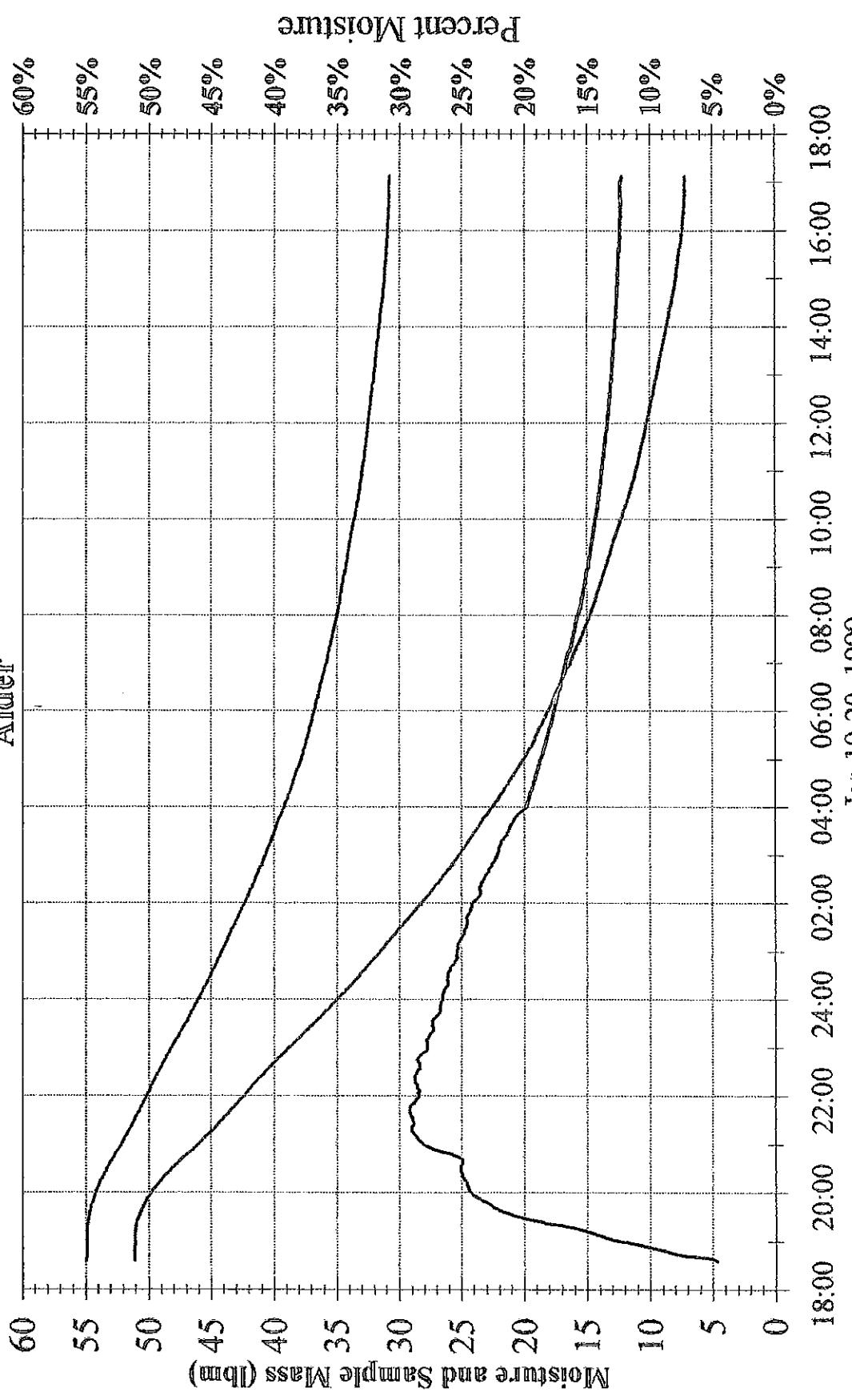
Northwest Hardwoods

Raw Data



Northwest Hardwoods

Alder



ALDER21.WB1

— Determinated Wet Bulb — Wood Sample Moisture — Wood Sample Mass

Horizon Engineering

03/15/99 16:22

CALIBRATION INFORMATION

Thermocouple Calibration

Date:	24-Mar-98	Deviation	@60 F	7.8 Allowable Diff.	Pb=	29.88 In Hg	JDF	
Test Calibration:	20-Sep-98	Limit	@212 F	10.1 Allowable Diff.	Ta=	70.0 oF	9803241c	
			@325 F	11.8 Allowable Diff.		<th></th>		
	Probe/ID	Ambient		Boiling, Water		Boiling, Oil		
		Standard, F	Measured, F	Difference F	Standard, F	Measured, F	Difference F	Average Difference F
Probe	3-1	33.2	33.0	0.2	211.4	211.4	0.0	-0.6 -0.13
Probe	3-2	33.2	33.4	-0.2	212.6	213.6	-1.0	352.8 356.8 -4.0 -1.73
Probe	3-3	34.8	34.8	0.0	210.6	212.6	-2.0	338.4 333.8 2.8 0.20
Probe	wc3-4	33.4	34.6	-1.2	212.2	214.2	-2.0	319.0 318.8 2.2 -0.33
Probe	3-5	33.2	33.4	-0.2	212.8	212.6	0.2	353.8 365.0 -11.2 -3.73
Probe	3-6	34.2	36.0	-1.8	211.6	213.8	-2.2	329.0 334.0 -5.0 -3.00
Probe	3-7	33.2	33.0	0.2	212.8	214	-1.2	358.6 358.8 1.8 0.27
Probe	3-8	33.2	33.6	-0.4	212.8	211.8	1.0	358.2 361.4 -3.2 -0.87
Probe	4-1	35.0	34.6	0.4	211.8	215	-3.2	346.6 346.8 -0.2 -1.00
Probe	4-2	34.6	33.0	1.6	211.2	208.2	3.0	332.4 328.4 4.0 2.87
Probe	4-3	35.4	36.2	-0.8	210.8	211.8	-1.0	332.8 336.0 -3.2 -1.67
Probe	4-4	34.4	33.2	1.2	210.6	211.6	-1.0	340.8 340.8 0.0 0.07
Probe	4-5	34.2	34.6	-0.4	210	212.2	-2.2	338.2 340.0 -1.8 -1.47
Probe	4-6	34.4	33.8	0.6	210.2	210.2	0.0	334.0 332.6 1.4 0.67
Probe	4-7	35.0	35.0	0.0	210.6	212.2	-1.6	336.4 340.4 -4.0 -1.67
Probe	5-2	33.0	33.8	-0.8	212.4	210	2.4	318.4 309.2 7.2 2.93
Probe	5-3	33.6	33.6	0.0	214.6	210.6	4.0	316.0 310.0 6.0 3.33
Probe	5-4	33.0	32.0	1.0	212.4	210.6	1.8	315.8 311.0 4.8 2.63
Probe	5-5	32.2	33.0	-0.8	211.4	210.4	1.0	314.4 314.0 0.4 0.20
Probe	5-6	33.0	32.6	0.4	213	210.8	2.2	315.4 313.8 1.6 1.40
Probe	5-7	32.4	32.4	0.0	214.4	211.2	3.2	319.6 317.4 2.2 1.60
Probe	5-8	33.0	32.8	0.2	212.4	211	1.4	324.4 321.8 2.6 1.40
Probe	5-9	33.0	32.6	0.4	212	211.2	0.8	317.4 320.0 -2.6 -0.47
Probe	7-1	33.6	32.6	1.0	210.8	210.8	0.0	313.0 315.8 -2.8 -0.60
Probe	7-2	33.6	33.0	0.6	211.8	211	0.8	318.6 318.6 0.0 0.47
Probe	7-3	33.2	33.6	-0.4	213.8	211	2.6	318.4 316.0 2.4 1.63
Probe	7-4	33.6	33.6	0.0	212.8	211.2	1.6	315.0 313.0 2.0 1.20
Probe	7-5	32.8	32.6	0.2	213.8	211.2	2.4	320.4 312.0 8.4 3.67
Probe	7-6	32.8	33.0	-0.2	213.4	211.6	1.8	312.4 311.8 0.6 0.73
Probe	10-1	33.6	33.6	0.0	211.8	211.8	0.0	317.2 315.6 1.6 0.63
Probe	10-2	33.8	33.2	0.6	213.8	211	2.8	315.4 316.2 -0.8 0.87
Pilot	10-3	33.2	34.4	-1.2	212.2	212.4	-0.2	315.6 318.4 -2.8 -1.40
Pilot	11-S	34.2	33.6	0.6	212.4	214.2	-1.8	314.8 314.2 0.6 0.20
Pilot	10-S	33.8	33.4	0.4	212.4	213.8	-1.4	325.2 319.0 6.2 1.73
F3	36.0	34.6	1.4	210.4	211.8	-1.4	280.8 278.6 2.2 0.73	
F23	34.2	35.8	-1.6	210	212.6	-2.6	274.0 272.0 2.0 -0.73	
F51	34.0	34.2	-0.2	211.4	211.8	-0.4	319.0 320.0 -1.0 -0.53	
F84	35.4	33.8	1.6	211.2	213.6	-2.4	308.2 311.8 -3.6 -1.47	
F85	35.2	33.8	1.4	211.2	213	-1.8	306.8 304.2 2.6 0.73	
F100	34.0	34.0	0.0	212.2	211.8	0.4	318.8 316.6 2.2 -0.87	
A1	33.2	32.6	0.6	210.8	211.6	-0.8	370.8 368.8 2.0 0.60	
A2	33.4	34.0	-0.6	212	211	1.0	370.4 367.4 3.0 1.13	
A3	33.2	33.8	-0.6	213	212	1.0	368.0 368.8 -0.8 -0.13	
A4	33.4	33.2	0.2	212.8	212	0.8	366.2 363.4 2.8 1.27	
A5	33.4	33.0	0.4	211.8	212.6	-0.8	364.8 362.8 2.0 0.63	
A6	33.2	33.8	-0.6	212.4	209.8	2.6	364.2 357.0 7.2 3.07	
B3	35.8	35.2	0.6	210.6	203.8	6.8	294.8 295.4 -0.6 2.27	
B7	36.2	35.0	1.2	211.2	201.6	9.6	287.4 290.6 -3.2 2.53	
B8	36.2	34.6	1.6	211.4	210.6	0.8	322.8 325.6 -2.8 -0.13	
B10	35.8	35.2	0.6	211.4	213.4	-2.0	312.8 314.8 -2.0 -1.13	
B11	36.2	35.4	0.8	211.2	208.4	2.8	328.0 328.6 -0.6 1.00	
B13	36.0	33.8	2.2	212	211.4	0.6	316.2 316.4 -0.2 0.87	
B14	35.6	34.3	1.3	211.4	213	-1.6	301.8 304.2 -2.4 -0.80	
AVERAGE		34.0	33.8	0.2	211.9	211.4	0.5	0.4
				0.04%		0.07%		0.06%
Tivoli Dial Gauges								
911B		35.4	35	0.4				
D-2					211.6	211	0.6	320.6 326.0 -5.4
D-6					211.4	210	1.4	322.0 330.0 -8.0
D-7		35.2	35	0.2	211.4	206	5.4	
D-8					211.2	210	1.2	321.8 328.0 -6.2
D-10		33.4	36	-2.6	210.6	212	-1.4	
D-14		36.2	32	4.2				

Standard Used Fluke 5895570

Thermocouple Indicator Calibration

AVERAGE 112.09 112.81
Standard used, fluke 5895570 calibrated 4-1-98 by Grant Edgley Co.

TEST METHOD

Test Method for Determination of Dry Kiln VOC Emissions

April 5, 1996

Prepared by:



and

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9-July-96**

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1.0 INTRODUCTION

Lumber dry kilns have been identified by the EPA and other environmental agencies as a source of Volatile Organic Compounds (VOCs). The green lumber contains VOCs, which are emitted during the drying process. In order to measure the emissions from dry kilns, it is recommended to apply a test method incorporating EPA Method 25A. However, it is not practical to use the standard EPA Method 25A for dry kilns, because of the following conditions:

- a.) Lumber drying can take over 100 hours to process one load.
- b.) Most dry kilns have multiple vents and often have significant leakage around the loading doors.
- c.) The venting process is periodic. The vents open to release moisture and VOCs in an irregular pattern.

The multiple vent configuration of most dry kilns and the periodic venting makes it difficult to measure the exhaust flow rate. The leakage from doors and other gaps is not measurable and therefore will produce inaccurate results. In addition, tests would need to be repeated for every species of wood the plant dries.

This method applies EPA Method 25A in a controlled environment, where a sample of the lumber is dried in a laboratory dryer and the VOC emissions are measured. The measured quantity of emissions can then be applied to determine accurate emission factors for the actual process by mathematical methods.

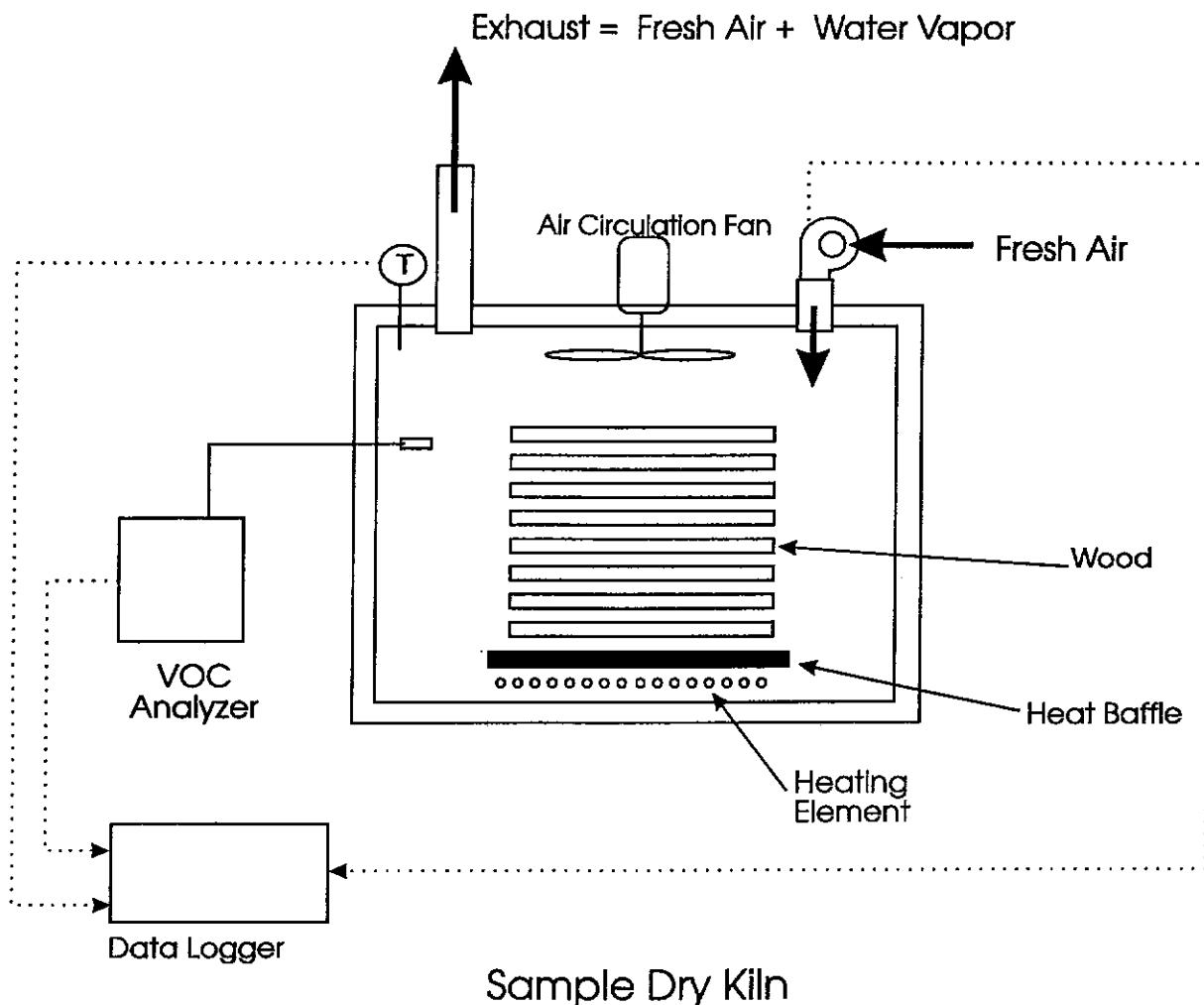
1.1 PRINCIPAL

The method for VOC measurements is based on simulated drying conditions in a laboratory size lumber dry kiln that operates in a controlled environment and can dry approximately 10 to 15 board foot of lumber.

The method is considered to be a worst case analysis, where the highest temperature for a typical drying cycle is applied to the sample at all times. The humidity is not controlled. The maximum temperature is to be that used at the actual kiln site. This is normally about 200°F. This method allows any sample drying time, but normal times of approximately 36 to 48 hours will result in a stable (dry) test load weight. Testing times can be extended if the test load weight is not stable. VOC concentrations from the test kiln are not expected to reach zero near the end of the drying cycle.

The VOC analyzer indicates concentration on a wet basis. To correct the concentration to a dry basis it is not necessary to continuously measure the moisture content of the sample stream even though the moisture varies over the drying cycle. An average moisture content for VOC analyzer correction is calculated at any time based on the dry air volume delivered to the kiln and the amount of moisture evaporated from the sample load. As long as the air flow rate to the kiln is greater than that extracted by the analyzer, moisture and air escaping from the oven through cracks are not a problem.

1.2 SYSTEM SCHEMATIC



1.3 APPLICABILITY AND SENSITIVITY OF RESULTS

From the laboratory test results emission factors can be calculated for a typical drying schedule. Separate emission factors can be calculated for each wood species to any percentage dryness.

1.4 TEST KILN APPARATUS

Test Kiln: Industrial drying oven, convection type, with sealed doors and openings, of a size sufficient to hold the test load with adequate air circulation space around the test load. The kiln shall be equipped with the following instrumentation:

Load Cell and Platform: The entire test load shall be sensed by the load cell on a continuous basis. The load cell suspension system shall be designed to minimize binding. The platform should allow the use of non-organic sticker boards to separate the test load boards in a manner similar to actual drying conditions.

Temperature Sensor: A continuous record of the kiln temperature shall be maintained.

VOC Sample Probe: A stainless steel or glass probe to gather sample for the analyzer. The probe outlet should be kept to a minimum length and insulated to prevent condensation before the heated sample line connection.

Air Inlet: To be placed in a location where the air becomes mixed quickly with oven internal air.

Air Outlet: A pressure relief line to allow excess exhaust air to vent. This line should be heated or kept sloped down to prevent accumulation of condensed water vapor that could block the exhaust stream.

Other Test System Equipment Necessary:

Total Hydrocarbon Analyzer System: Heated total hydrocarbon analyzer and sample line, constructed, operated, and calibrated according to EPA Method 25A.

Inlet Air System: A system of providing a constant, measured, hydrocarbon free air to the system. The air should either be dried or have its temperature and humidity measure so that moisture in the stream can be quantified.

Data Logging System: A system to provide a continuous record of the recorded parameters throughout the testing period. Data is to be recorded at intervals no longer than two minutes apart.

2.0 SAMPLE COLLECTION PROCEDURE

Depending on the species and on the location of the board within the log, the VOC content will vary. It is recommended that the collected samples represent a cross section of the log from which the board were cut.

Resin rich soft woods often have localized pitch concentration. These so-called pitch pockets can release significantly more VOC than the average board. Sample boards with pitch pockets should not be selected for the test batch of lumber.

Each species of lumber must be tested separately in order to determine species specific VOC release. Therefore all sample boards for a specific test must be of the same species.

The selected boards must be cut into sample boards between 18" and 24" long (all samples boards should be of approximately the same length).

The board thickness and the width of the boards must represent the average dry kiln load.

The samples must be collected immediately after the log is sawed into boards (within 8 hours).

At least 6 separate boards must be used to compile the sample load.

The composite sample load must be at least 10 board foot based on U.S. Lumber Scale.

Each board must be marked with the date of collection, a batch number and a board number (example - Mar 20/96 - 1/3). This means that the piece came from the first of the six selected boards and is the third piece of the same board. It is best to use pencil for marking. Marking pens may add VOCs to the board.

After the sample board are collected, prepare a data sheet with the following information:

- a.) Company Name
Address
Telephone Number

(OGC Test Report Sample Copy Right © 1996 by the Oregon Hardwood Council)

Contact Person

- b.) Date of sample preparation.
Responsible person collecting the sample.
Signature of the responsible person.
- c.) Species of the lumber.
- d.) Total number of pieces shipped and the total board feet in the sample batch.
- e.) Dry kiln identification in which this lumber is normally dried.
Identify more than one kiln, if appropriate.
- f.) Identify each sample piece as shown in the following example:

<u>Sample #</u>	<u>Nominal Size</u>	<u>Length</u>
1/3	8/4" by 6"	18" (plus or minus 1/8")

- g.) Provide the normal drying schedule for this lumber and the maximum drying temperature.
- h.) Provide the final moisture content for this lumber.

Immediately after collecting the samples the entire package of sample boards must be shrink-wrapped or enclosed in a plastic bag and sealed with tape to avoid moisture and VOC loss.

2.1 SAMPLE SHIPPING PROCEDURE

The samples should be packaged in a box to avoid damage of the vapor seal during shipping. To ensure arrival at the laboratory within 48 hours of the date the samples were cut and wrapped, select a carrier that can deliver within the specified time.

2.2 PREPARATION AND SET-UP BEFORE TESTING

The testing laboratory must be prepared to perform the test within 96 hours after the samples were collected. Samples should be refrigerated in the shipping materials until the testing is started.

(Redacted)

The VOC analyzer must be calibrated following EPA Method 25A. The load cell must be calibrated with known weights. The oven should be preheated for several hours at a temperature slightly above the anticipated test maximum to avoid condensation.

After the preparation, place the lumber in the sample dry kiln and start the VOC sampling device. After the drying cycle has been started, the sample kiln door must be latched and may not be opened during the entire drying process.

The lumber in the sample dry kiln must be dried to the maximum temperature at which the lumber is normally dried at the plant site. Test kiln temperature may be increased at intervals, however, to avoid very high humidity in the chamber.

The heating system and internal air circulation system for the dry kiln must be operating continuously during the drying process.

2.3 DATA COLLECTION

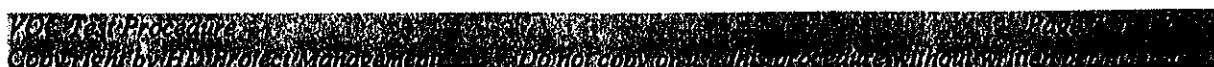
During the drying cycle the following information shall be collected and recorded.

- a.) VOC concentration, in ppmvC, inside the sample dry kiln once every two minutes.
- b.) The temperature in the sample dry kiln.
- c.) The in-flow of fresh air into the sample dry kiln in scfh. The flow rate shall not be less than 10 scfh and not more than 100 scfh for every 10 board foot of lumber in the sample kiln. The meter temperature and the relative humidity of the in-flow air should be recorded.
- d.) The weight of the lumber once every two minutes.
- e.) The total drying time in hours and minutes shall be recorded.

2.4 TERMINATING THE DRYING CYCLE

The lumber will be dried until the weight of the wood has become stable to less than +/- 0.25 lb over a 12 hour period. Some variation in weight can be expected due to inlet air humidity changes.

Final calibrations checks should be conducted on the VOC analyzer as outlined in EPA Method 25A. A post check on the weighing system must also be performed.



3.0 DATA EVALUATION THEORY

The air in-flow rate and the total air flow data for the entire cycle will be the summarized meter reading in cubic feet. The air in-flow corrected to a dry standard (dscf) will be the same as the out-flow dscf. This will be the volume used in the pounds of VOC calculation.

The water vapor volume will be calculated from the total water loss of the sample plus the water introduced in the in-flow air. From the total water vapor volume and the total dry air volume a percentage moisture can be calculated for any time during the test cycle.

With the results of VOC concentration in ppmvC (wet basis), the percentage moisture, and the volumetric flow in dscf, the total VOC release in lbC can be calculated for any lumber moisture content.

From the result in lb of VOC for the test sample, an emission factor in lb of VOC per 1000 board feet of lumber can be calculated.

3.1 EQUATIONS TO DETERMINE EXHAUST FLOW

The actual exhaust flow from the sample dry kiln is the sum of the air flow plus the water vapor flow from the evaporated water in the wood. However, this is not used in the emission factor calculation.

a.) Air in-flow in dscf

$$V_{sd} = Y V_m T(\text{std}) P_b m_{fg}(2) / P(\text{std}-1) T_m(\text{abs})$$

V_m = meter reading volume in actual cft

Y = gas meter correction factor

T(std) = standard temperature, 527.67°R

T_m(abs) = meter temperature in degree Rankin.

P_b = pressure in inch Hg at test site.

P(std-1) = standard pressure, 29.92129 inHg

m_{fg}(2) = mole fraction of dry meter air

b.) Mole fraction of dry meter air

$$m_{fg}(2) = 1 - B_{ws}(2)/100$$

$$Bws(2) = RH Vp / Pb(2)$$

Bws(2) = percent moisture of in-flow air

RH = relative humidity of in-flow air

Vp = vapor pressure of moisture content of in-flow air

Pb(2) = barometric pressure in kPa

c.) Vapor pressure of moisture content of in-flow air

$$Vp = \exp(A + B Tm + C/Tm + D/Tm^2)$$

A = 18.6866

B = -0.00243724

C = -4509.47

D = -149541.0

*in this equation Tm is in °C + 273.15

3.2 EQUATION TO DETERMINE EXHAUST MOISTURE

a.) Mole fraction of dry gas

$$mfg(1) = 1 - Bws(1)/100$$

Bws = percent moisture of exhaust

b.) Percent moisture

$$Bws(1) = 100 Vw(std) / Vw(std) + Vm(std)$$

Vw(std) = volume of water vapor, scf

Vm(std) = volume of dry gas, scf

c.) Volume of water vapor

$$Vw(std) = 0.04707 W / 0.99823 + Vw(std)_{in} + Vw(std)_{initial}$$

W = weight loss of wood, grams

Vw(std)_{in} = volume of water vapor in the in-flow gas, scf

Vw(std)_{initial} = volume of water vapor in over at start of test

3.3 VOC CONCENTRATION

a.) VOC concentration corrected

VOC(cor) = VOC(dry) corrected for drift per EPA Method 25A

b.) VOC dry calculation

VOC(dry) = VOC(wet) / mfg(1)

VOC(wet) = average from analyzer in ppm

mfg(1) = mole fraction of dry air in oven

3.4 TOTAL SAMPLE VOC IN POUNDS

Mgas = VOC(cor) MW Pstd(2) Vsd / 1000000 R T(std)

VOC(cor) = ppm dry, corrected for drift

MW = molecular weight of carbon, 12.01 lbm / lbmol

Pstd(2) = 2116.22 lbf / ft²

Vsd = volume of sample (section 3.1)

R = 1545.33 ft lbf / lbmol °R

T(std) = absolute standard temp., 527.67 °R

3.5 VOC EMISSION FACTOR

It is recommended to express the VOC emission factor is in Lbs. of VOC per 1000 board foot of lumber based on U.S. lumber scale. For other lumber scales the numbers must be corrected.

a.) Emission factor in Lbs./1000 BF (U.S.)

EF = Mgas / (BF_{sample}) * 1000 (in Lb / 1000 BF U.S.)

BF = Total board foot of lumber dried in the sample kiln in U.S. lumber scale.